UNCLASSIFIED

AD NUMBER AD880676 LIMITATION CHANGES TO: Approved for public release; distribution is unlimited. FROM: Distribution authorized to U.S. Gov't. agencies and their contractors; Critical Technology; NOV 1970. Other requests shall be referred to U.S. Army Aviation Materiel Laboratories, Fort Eustist Virginia 23604. This document contains export-controlled technical data. **AUTHORITY** USAAMRDL ltr, 10 Sep 1971



USAAVLABS TECHNICAL REPORT 70-1B HELICOPTER ROTOR ROTATIONAL NOISE PREDICTION AND CORRELATION

VOLUME II

DOCUMENTATION OF NOISE PREDICTION COMPUTER PROGRAM

By

Ronald G. Schlegel

William E. Bausch

November 1970

U. S. ARMY AVIATION MATERIEL LABORATORIES FORT EUSTIS, VIRGINIA

CONTRACT DA 44-177-AMC-448(T)
SIKORSKY AIRCRAFT
DIVISION OF UNITED AIRCRAFT CORPORATION
STRATFORD, CONNECTICUT

This document is subject to special export controls, and each transmittal to foreign governments or foreign nationals may be made only with prior approval of U.S. Army Aviation Materiel Laboratories, Fort Eustis, Virginia 23604.

OD

U.S. Army Aviation Materiel Laboratories has been redesignated Eustis Directorate, U.S. Army Air Mobility R&D Laboratory per CG 281. The old name has been used here to agree with what is on the report.

82

DISCLAIMERS

The findings in this report are not to be construed as an official Department of the Army position unless so designated by other authorized documents.

When Government drawings, specifications, or other data are used for any purpose other than in connection with a definitely related Government procurement operation, the United States Government thereby incurs no responsibility nor any obligation whatsoever; and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data is not to be regarded by implication or otherwise as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission, to manufacture, use, or sell any patented invention that may in any way be related thereto.

DISPOSITION INSTRUCTIONS

Destroy this report when no longer needed. Do not return it to the originator.



DEPARTMENT OF THE ARMY HEADQUARTERS US ARMY AVIATION MATERIEL LABORATORIES FORT EUSTIS, VIRGINIA 23804

This contract was initiated to acquire NH-3A/S-61F helicopter noise measurements simultaneously with low- and high-frequency aerodynamic rotor loads for the purpose of verifying the accuracy of a rotational noise prediction program. The program itself was modified from the previously assumed rectangular chordal airload distribution to the actual measured chordal airload distribution or to any arbitrary chordal distribution that the program user wished to assume.

Results of this contract demonstrate the importance of high-frequency airloads and the chordal airload distribution in rotational noise predictions. Although inconclusive regarding how many loading harmonics are necessary, findings do show that knowledge of the chordal airload distribution can compensate for a lack of high-frequency airload data.

There are a few available analytical solutions to helicopter rotational noise in addition to that reported herein. These analyses vary in rigor of approach, degree of difficulty of usage, and quantity of input data required, but all appear to be uniformly accurate for the first three or four harmonics of rotational noise under the few normal rotor operating conditions examined.

A program is currently under way to: (1) simultaneously acquire noise and rotor airloads data for "slapping" and "nonslapping" flight conditions of a CH-53A helicopter and (2) correlate these data with noise and airloads prediction methods. The acoustic analyses presented herein will be modified and used in an attempt to predict the occurrence of impulsive rotor noise.

Task 1F162203A14801 Contract DA 44-177-AMC-448(T) USAAVLABS Technical Report 70-1B November 1970

HELICOPTER ROTOR ROTATIONAL NOISE PREDICTION AND CORRELATION

Final Report

Volume II

DOCUMENTATION OF NOISE PREDICTION COMPUTER PROGRAM

Вy

Ronald G. Schlegel

William E. Bausch

Prepared by

Sikorsky Aircraft
Division of United Aircraft Corporation
Stratford Connecticut

For

U. S. ARMY AVIATION MATERIEL LABORATORIES FORT EUSTIS, VIRGINIA

This document is subject to special export controls, and each transmittal to foreign governments or foreign nationals may be made only with prior approval of U.S. Army Aviation Materiel Laboratories, Fort Eustis, Virginia 23604.

ABSTRACT

A computer program for rotational noise prediction is documented in the following sections of this report. The program was developed as a part of a study to develop more accurate methods for predicting rotational noise levels under conditions of nonuniform inflow over the rotor disc.

The computer program will calculate the root-mean-square sound pressure level for up to the 10th harmonic of rotor noise at any field point in the near or far field outside of the rotor disc. Noise levels can be calculated either from a rectangular chordwise distribution of pressure or from the measured chordwise distribution. The equations for noise prediction using the arbitrary (measured) chordwise distribution are derived in Volume I of this report. Although this report concentrated on a helicopter rotor, the analytical results are applicable to propellers in general.

FOREWORD

A computer program for rotational noise prediction was written by Sikorsky Aircraft, Division of United Aircraft Corporation, as part of Contract DA 44-177-AMC-448(T), Task 1F162203A14801. USAAVLABS Project Engineer was Mr. Joseph H. McGarvey.

Acknowledgement is made to Mr. Gediminias Campe for his help in designing the computer program and in bringing it to operational status.

TABLE OF CONTENTS

	PAGE
ABSTRACT	iii
FOREWORD	. v
LIST OF ILLUSTRATIONS	viii
INTRODUCTION	. 1
PROGRAMMER/USER INFORMATION	. 2
HARDWARE AND SOFTWARE REQUIREMENTS	. 2
PROGRAM DESCRIPTION	. 2
Subroutines	. 2
Overlay Structure	. 3
Program Symbols	. 3
Input/Output	11
Operating Instructions	11
Program Logic	13
Program Equations	13
Program Listing	15
Limitations of the Program	15
DISTRIBUTION	72

LIST OF ILLUSTRATIONS

FIGURE		PAGE
1	Sample Input, Symbolic	16
2	Sample Input, Numeric	18
3	Sample Output	. 21
4	Coordinate Systems for Noise Prediction	. 37
5	Program Listing - Main	. 38
6	Program Listing - Main	. 39
7	Program Listing - Main	. 40
8	Program Listing - Main	. 41
9	Program Listing - Main	. 42
10	Program Listing - Main	. 43
11	Program Listing - Main, Noise Analysis Begins	. 44
12	Program Listing - Main	. 45
13	Program Listing - Main	. 46
14	Program Listing - Main	. 47
15	Program Listing - Main	. 48
16	Program Listing - Main, CURVIT	. 49
17	Program Listing - CURVIT	. 50
18	Program Listing - CURVIT, RDKU	. 51
19	Program Listing - RDKU, INTERP	. 52
20	Program Listing - INTERP, MERGES	• 53
21	Program Listing - MERGES	. 54
22	Program Listing - MERGES, DFSRIE	. 55
23	Program Listing - DFSRIE, CUE	. 56
24	Program Listing - CUE, BLODAT	. 57

LIST OF ILLUSTRATIONS

FIGURE	<u>P</u> #	AGE
25	Program Listing - BLODAT, INPUTA	58
26	Program Listing - INPUTA 5	59
27	Program Listing - INPUTA, UNPACK	60
28	Program Listing - UNPACK, PARAM 6	51
29	Program Listing - PARAM, TRIDAG	52
30	Program Listing - TRIDAG 6	53
31	Program Listing - TRIDAG, CUBIC	54
32	Program Listing - CUBIC, OUTSPL 6	55
33	Program Listing - OUTSPL, AVQUAD6	66
34	Program Listing - AVQUAD, E386RN6	57
35	Program Listing - E386RN	68
36	Program Listing - E386RN, SIMCOR	59
37	Program Listing - SIMCOR, START, CLOCK	70
38	Program Listing - CLOCK, END	71

INTRODUCTION

This report describes a computer program for calculating noise harmonic levels of rotor (or propeller) rotational noise at any point in the acoustic near or far field. In order to simplify the analysis, noise due to blade thickness and aerodynamic shears is not considered, and the rotor disc is assumed to be a flat circular plate perpendicular to the thrust of the rotor system.

The basic physics of the noise prediction analysis are straightforward. Acoustic dipoles (sources and sinks) are the mathematical models used to describe the pressure variations caused by a rotor blade passing over any given point in the rotor disc. By applying an acoustic wave equation, the pressure variations at this point in the disc are transformed to a rotational noise component at a particular field point or observer location. In order to calculate the net rotational noise for a given harmonic and field point, the contributions of many points in the rotor disc are added (vector addition with magnitude and phase) to produce the root-mean-square sound pressure level (SPL) in decibels (dB).

The form of the pressure pulse seen by a point in the rotor disc is important in determining how much noise will be generated. The noise prediction program is designed to use a pulse of arbitrary form, namely the measured chordwise distribution of differential pressure on the section of rotor blade that passes over the point of interest in the rotor disc.

PROGRAMMER/USER INFORMATION

HARDWARE AND SOFTWARE REQUIREMENTS

The noise prediction computer program is written in FORTRAN V for a UNIVAC 1108 digital computing system. In order to manipulate all of the data generated by the program, direct-access storage devices are used. These devices should be UNIVAC FH-332 drums, each with a capacity of at least 90,000 words. Three drum units are called by the program.

PROGRAM DESCRIPTION

The following sections of this report describe the subroutines, structure, and running of the noise prediction computer program.

Subroutines

The name and function of each of the program subroutines are listed below. During normal operation, i.e., all input data on punched cards, the subroutines dealing with magnetic tape will not be called by the main program

E676 Main program, calculates SPL based on the actual chordwise distribution of pressure.

BLODAT BLOCK DATA subroutine.

RDKU Reads in one record from the proper input tape, where two records make up one azimuthal pressure cycle.

UNPACK Unpacks an array containing tape information (two records) into separate arrays representing azimuthal pressure cycles for each pressure transducer channel.

INTERP Linearly interpolates pressure pulse harmonics up to 20 blade span stations and 288 azimuths.

CUE Calculates an array which is a function of azimuth and blade station. A double integration of this variable yields the sound pressure components Um and Vm.

INPUTA Reads and prints out card input.

MERGES Combines the absolute pressure of the instrumented top and bottom blade stations, to produce only differential pressures for all blade stations.

OUTSPL Output subroutine.

DFSRIE Computes the coefficients of a Fourier series.

AVQUAD Performs integration by averaged quadratics based on Lagrange interpolation.

E386RN Calculates SPL based on a rectangular chordwise distribution of pressure.

SIMCOR Simpson's Rule integration subroutine.

CURVIT Cubic interpolation subroutine.

PARAM Subroutine used by CURVIT.

CUBIC Subroutine used by CURVIT.

TRIDAG Subroutine used by CURVIT.

START Initializes the clock subroutine CLOCK.

CLOCK Calls the computer clock for the time.

Overlay Structure

In order to pack the data and processing instructions into the memory of the UNIVAC 1108, an overlay technique was used. The overlay map is given below. The small "b" indicates a blank space on the punched card.

bbMAPbE676,, OVER

bbbbbbsegbe676-(*E386RN, *ALPHA)

ALPHAbbsegb*RDKU-*UNPACK-*INTERP-*CUE-*INPUTA-*MERGES-*OUTSPL-*DFSRIE

7/8babsbover, AE676

7/8bXQTbCUR

Program Symbols

Both the definition of the alpha-numeric symbols and their proper input units are indicated below. These symbols are used in the programmed equations and in the sample input that are presented later in this report. During normal operation, only those symbols under CARD INPUT need to be included in the input data set.

TAPE INPUT	CARD INPUT	PROGRAM SYMBOL	UNITS	DESCRIPTION
ХХ	X	BB .	in.	Blade thickness; floating point
хх	X	AA	in.	Blade chord; floating point
xx	x	BLADEL	in.	Length of blade (root to tip); floating point

			•	
TAPE INPUT	CARD INPUT	PROGRAM SYMBOL	UNITS	DESCRIPTION
XX	X	GAMA	deg/in.	Twist rate of main rotor blade; floating point
XX	Х	RO	in.	Radial station with zero twist; floating point
XX	X	CC	in./sec	Speed of sound; floating point
XX	X	OMEG	rpm	Rotor rotational speed; floating point
XX	x	DPSI	deg	Delta azimuth angle=1.25° or a multiple of 2.5°. All calculations are done at this increment
XX	X	NBLADE		Number of main rotor blades; fixed point
XX	х	MLIMDP		Highest order of harmonic desired to represent all pressure cycles (=1 to 30); fixed point
XX	X	MLIMRN	v	Highest order of harmonic desired in the rotor noise calculations (=1 to 10); fixed point
XX	x	LSPAN		The number of radial stations as a result of interpolation (=10 or 20). This is an option
XX	X	IREELS		Total number of reels (up to 5)
XX -	X .	TCOP		■TAPE, data will be read from tape
		• •		=CARD, data will be read from cards
XX	x	PUNCH		=YES (option to punch out pressure cycle coefficients)
XX	X	INTERM		<pre>Intermediate output to be used for checkout; =YES or = NO</pre>
XX	, X	IDD		Debug printout option; = 0, do not print; =1, print
XX	X ,	E3860P		=YES, call rotor noise subroutine E386RN =NO, do not call E386RN

TAPE INPUT	CARD INPUT	PROGRAM SYMBOL	UNITS	DESCRIPTION
XX	х	OPRONO		Option to calculate SPL from actual chordwise loading =YES, perform rotor noise program =NO, go to subroutine E386RN
XX .	X	NFT		Number of field points (up to 20); fixed point
хх	Х	ANG	deg	Increment of integration used in E386 subroutine; floating point
XX	X	NHH		Number of Air Load harmonics for E386 program (up to 30); fixed point
XX XX	X X	KEY3 KEY2 KEY1		=99, have intermediate output from the E386 program =00, no intermediate output
XX XX XX	X X	CAPRF(I) THETAF(I) ALFAF(I)	ft deg deg	Spherical coordinates of field point I, used in subroutine E386RN; floating point
XX XX XX	X X	XFP(I) YFP(I) ZFP(I)	in. in. in.	Coordinates of field point I, origin being at center of rotor disc (I=variable= 1 to 20); floating point
XX	X	IBURST		Burst number being processed, identifies data on telemetry tape
	X	ВО	deg	Collective pitch angle; floating point
	X	BIC	deg	Longitudinal cyclic pitch; floating point
	x	BIS	deg	Lateral cyclic pitch; floating point
	x	IN		Spanwise station number, fixed point
	X	JN		Chordwise station number, fixed point
1	X X	CN(I,JN,IN) SN(I,JN,IN)	psi psi	Fourier coefficients of differential pressure where: I = harmonic, JN= chord, IN= span

	CARD INPUT	PROGRAM SYMBOL	UNITS	DESCRIPTION
XX	1	SLOPE(I,K)		Conversion factors used to get the
XX	(OFFSET(I,K)	psi	tape data into engineering units for each tape parameter. I = channel number, K = reel number
XX		KUNIT(I)		Tape drive units on which to mount tape reels
XX		IREEL		Input tape reel number
XX		NC		Channel number
XX		NTBDX(I,J)		Designates top or bottom pressure gage I = IREEL, J = NC
XX		NSTATC(I,J)	Relative chordal position of pres- sure gage from leading edge (=1,2,3,4,5). I=IREEL, J = NC
XX		NSTATR(I,J)	Relative radial station measured from root of blade (=1,2,3,4,5) I = IREEL, J = NC
xx		NCEND		Input control word. When NCEND is not blank, card specifying reel number follows
xx		ISET(I)		Set number for reel IREEL
XX		FROC(K)		Filter roll-off correction curve, where K represents the order of the loading harmonic (K= 1 to 30)
		Q1(288,20) Q2(288,20) Q3(288,20)		Functions used in the double integration
		UMF(10,20) VMF(10,20)		Components of sound pressure
		PMRMS(10,20	o)	Sound pressure
		SPLM(10,20)	Sound pressure level
		LAZI		The number of azimuth stations as a result of interpolation This is calculated knowing DPSI

TAPE INPUT	CARD INPUT	PROGRAM SYMBOL	UNITS	DESCRIPTION
		IRS(I)		<pre>Instrumented radial station counter, counting from blade root. If station N.G. then IRS(I) = 0</pre>
		ITRACK(I)		Track number for reel number I
		FI(I,J)		Gaussian integration factors for radial station I, chord station J
		NCHAN(I,L)		Blade instrumented station designation for radial station I, chord station J. If = 0, then that station is N.G.
		RR(I)	fraction	Fractional radial station measured from hub center. I = span station = 1 to 5
		XA(I,J)	fraction	Fraction of distance along chord from leading edge. J = span = 1 to 5, I = chord station = 1 to 5
		NCH(I)		Total number of chord stations for radial position I
		XLO(I) XLM(I,J) XMM(I,J)	lb/in. lb/in. lb/in.	Air Load harmonics used in subroutine E386 where: I = radial station and J = harmonic
		CHORD(I)	fraction	Chord station array used in the average quadratics integration to get Air Loads (I = chord)
		GPSI(I)	psi	Differential pressure array along a chord, used in average quadratics integration
		FN(I)		Temporary array used to store Air Loads just before harmonic analysis
		PI	rad	PI = 3.14159
		AZMTH2(I)	rad	Azimuth array 0 to 2π rad in (2.5 π /180) rad increments (I = 1 to 144)
		AZMTH(I)	deg	Azimuth array 0 to 360 deg in 2.5-degree increments (I = 1 to 144)

TAPE INPUT	CARD INPUT	PROGRAM SYMBOL	UNITS	DESCRIPTION
		AZMTH3(288)		Azimuth array every DPRAD radians from 0 to 2π
		DPRAD	rad	$\Delta \psi$ expressed in radians
		BLADES		Number of blades
		SPAN(L)	in.	Radial stations used in the double integration, L = 1 to 20
		S	in.	Distance from element of rotor disc to field point
		В	deg	Blade pitch angle
		GPSI1(I)	psi	Array used in integration of g_m (ψ ,R) and $h_m(\psi$,R)
		CHORD2(I)	fraction	Interpolated chord station array used in integration of $g_m(\psi,R)$ and $h_m(\psi,R)$
		AN(I,J,K) BN(I,J,K)		Cosine and sine Fourier coeffi- cients used in filter roll-off correction. I = harmonic, J = channel, K = reel
		TEM1(I) TEM2(I)		Temporary arrays used in Fourier analysis subroutine arguments
		AZRAD	rad	2.5° expressed in radians
		<pre>ichanl(1,J)</pre>		Tape channel designation, where $J = 1$ to NOCH(J) and $I = 1$ to IREELS
		NO YES		Control words used to check whether or not to execute an option
		NBLANK		Word with all blanks in it
		TEE		Equals "T" in Hollerith used to designate top of blade
		BEE		Equals "B" in Hollerith used to designate bottom of blade
		DEE		Equals "D" in Hollerith used to designate differential pressure

TAPE INPUT	CARD INPUT	PROGRAM SYMBOL	UNITS	DESCRIPTION
		COSINE(I)	deg	Cosine array defined every DPSI degrees
		SINE(I)	deg	Sine array defined every DPSI degrees
		AZ41(I)	rad	Azimuth points I along the chord for a given nominal azimuth
		NCYCLE		Cycles in a burst, counter
		CYCLES		Total number of cycles in a burst
		KU		Current tape unit number
		NDIV(4)		Used to shift integer numbers
		BMASK(6)		Used to mask out parts of a word
•		NOCH(I)		Total number of good channels on reel number I
		LIRS		Number of good radial stations
		FTRACK		Current track numbers being read from tape (2nd half of NN(217))
		FBURST		Current burst number being read from tape (2nd half of NN(218))
	- E	FREC		Current record number being read from tape (2nd half of NN(219))
		NN (435)		Tape data cycle array made up of 2 records (Last 3 words are control words)
	u .	ND1(I,J,K) ND2(I,J,K)		Unpacked raw data arrays where: I = azimuthal data point, J = chord station, K = radial station
	•.	DATA2(I,J,K)		Unpacked average raw data cycle where: I = data point, J = chord station, K = radial station
		DATAL(I,J,K)	psi	Scaled and corrected average pres- sure cycles where: I = data point, J = chord, K = radial station

TAPE INPUT	CARD INPUT	PROGRAM SYMBOL	UNITS	DESCRIPTION
		COSRN(I) SINRN(I)		Cosine and sine arrays, the elements being calculated at each instrumented chord station. Used in calculating Fourier coefficients of acoustic Air Loads
		GPSI2(I)	psi	Differential pressure array along a chord, used in average quadratics integration
		GMAR(I,K)		<pre>mth cosine coefficient of acoustic pressure pulse where K = radial station, I = azimuthal station</pre>
		HMAR(I,K)		<pre>mth sine coefficient of acoustic pressure pulse where K = radial station, I = azimuthal station</pre>
		DPSI1(I)	psi	Differential pressure array along chord, used in averaged quadratics integration
		GMARI(I,K)		mth cosine coefficient of acoustic pressure pulse after interpolation. I = up to 288, K = 10 or 20
		HMARI(I,K)		mth sine coefficient of acoustic pressure pulse after interpolation. I = up to 288, K = 10 or 20
		TEMP1(I) TEMP2(I) TEMP3(I)		Temporary work arrays used in the interpolation of GMAR and HMAR
		XO(I)		Arrays used in interpolation, I = 1 to 20
		W(I)		Temporary work array, I = 1,14
		NOPTS1		Number of radial stations before interpolation (including end points .194 and 1.0)(up to 7)
		ISI		ISI = (DPSI/2.5) > 1; if < 0 then ISI = 1
		POINT(15)		Gauss integration points (normalized)

TAPE INPUT	CARD INPUT	PROGRAM SYMBOL	UNITS	DESCRIPTION
		WPOINT(15)		Gauss integration weights
		NXY		Number of Gauss points and weights to be used
		PI2	rad	FI2 = 6.28318
		IX		The number of radial intervals to be used in the double integration
		IY		The number of azimuthal intervals to be used in the double integration

Input/Output

The input format is defined symbolically in Figure 1. Note that the blank lines are used to insure legibility. Normal input data would have no blank lines (unpunched cards) unless all of the parameters on a particular card happen to be equal to zero. Figure 2 is a sample numerical input for the first span station with 8 harmonics of pressure for each chord station. The format for the pressure harmonics CN(I,J,K) and SN(I,J,K) for the remaining span stations is completely analogous to that for Span 1. Span stations are specified from root to tip of the blade, and chord stations are specified from leading edge to trailing edge.

Normal output from the noise prediction program contains the following information:

- 1. Listing of the input parameters except the harmonics of pressure.
- 2. Values of differential pressure at each span and chord station every DPSI degrees of azimuth from the sum of the input pressure harmonics.
- 3. Field point coordinates and the corresponding predicted SPL for each noise harmonic.

A typical output is contained in Figure 3.

Operating Instructions

The noise prediction computer program has several options that may be selected. For normal operation, the print options for INTERM and IDD should be refused. If this is not done, several hundred pages of non-essential output will be generated. The following suggestions assume that the input pressure data are on punched cards so that option TCOP is equal to CARD (i.e., no data on magnetic tape).

The azimuthal increment of integration for E676 can be varied from 1.25 degrees to integral multiples of 2.5 degrees, while the value of ANG used in subroutine E386RN can be any value greater than 0.5 degree as long as

(360/ANG) is an even integer. Normally, DPSI and ANG should be equal. If only the first harmonic of noise is being calculated, an increment of 10.0 degrees is acceptable. If 4 harmonics of noise are desired, an increment of 2.5 degrees is recommended. The number of interpolated span stations can be 10 or 20. The larger is recommended for DPSI of 2.5 degrees or less.

Results presented in Volume I of this report demonstrate the importance of high-frequency loading harmonics for prediction of the higher harmonics of noise. At least 15 loading harmonics are recommended for calculation of up to the fourth noise harmonic. However, if only the level of the fundamental is desired, 2 or 3 loading harmonics probably will suffice.

Running time will be a function of the angular increment selected. Calculation of 4 harmonics of rotor noise at 20 field points from both the actual and the hypothetical rectangular chordwise pressure distributions requires approximately 6 minutes of machine time (excluding time for CUR instructions and compilation which can be on the order of 1 minute). Calculations with the actual chordwise distribution take roughly 5 minutes while the corresponding calculations with the rectangular distribution require approximately 1 minute. Running time increases as the azimuthal increment becomes smaller.

The coordinate system for E676 is right-handed Cartesian with Z positive up (in direction of rotor thrust), X positive aft, and Y positive to starboard. The origin of the system is at the center of rotation of the rotor. The coordinate system for E386RN is spherical in which R is the distance between the center of rotation and the field point, θ is the azimuth angle in the plane of the rotor disc, and σ is the elevation angle relative to the rotor disc (positive for field points above the disc). Figure 4 contains the coordinate systems for OPRONO and E386OP as used for a conventional helicopter rotor.

If the noise prediction program is used to calculate rotational noise for a propeller rather than a rotor, the following coordinate system definition applies. Z and σ are positive for field points on the positive thrust side of the rotor disc. The X-axis and θ = zero line coincide with the reference point for the azimuthal loading harmonics.

It is advisable to calculate rotational noise via both the OPRONO and E3860P options to determine if the loading details included in OPRONO need to be considered for the configuration being studied. If the rectangular chordwise loading distribution yields acceptable results, use E386 exclusively in order to save computing time.

Detailed instructions regarding control cards and execution commands must be provided by a programmer who is familiar with the particular UNIVAC 1108 installation that is to be used. When the input data and overlay structure are specified correctly, no problems should be encountered in running the program.

Program Logic

Program E676 proceeds as follows for card input (TCOP = CARD):

- 1. Accept harmonics of differential pressure from cards. Sum these harmonics to produce the differential pressure at each span and chord station every DPSI degrees of azimuth.
- 2. If output from E386 is desired, calculate the blade section loading (pounds per inch of span) by integrating the differential pressures across the chord at each span station. A trapezoidal integration routine is used.
- 3. Proceed through E386.
- 4. If noise levels based on the actual chordwise pressure distribution are required, interpolate to provide 41 points along the blade chord. These points are required to define the Fourier coefficients of the pulse shape (chordwise pressure distribution).
- 5. Calculate GMAR and HMAR for a particular noise harmonic.
- 6. Interpolate GMAR and HMAR if 288 azimuthal points and 20 radial points are desired. This interpolation produces GMARI and HMARI.
- 7. Calculate CUE array for the first field point.
- 8. Calculate UMF and VMF components of sound pressure for the first field point.
- 9. Calculate SPLM for the first field point.
- 10. Repeat steps 7, 8, and 9 for the rest of the field points (field point loop).
- 11. Repeat steps 5 through 10 for the rest of the noise harmonics (harmonic loop).
- 12. Repeat steps 1 through 11 for the remaining flight conditions or "data bursts" (burst loop).

Program Equations

Volume I of this report contains the derivation of the noise prediction equations. The critical parameters are GMARI, HMARI, S, Q1, Q2, Q3, UMF, VMF, PMRMS, and SPLM. The relationship between these program symbols and their engineering counterparts is:

$$GMARI = g_{m}$$

$$HMARI = h_{m}$$

$$S = s$$

$$Q1 = rq_1$$

$$Q2 = Q1q_2$$

$$Q3 = Q1q_3$$

$$\begin{aligned} & \text{UMF} &= \text{U}_{\text{m}} \\ & \text{VMF} &= \text{V}_{\text{m}} \\ & \text{PMRMS} &= \text{P}_{\text{m}} \\ & \text{SPLM} &= \text{SPL}_{\text{m}} \end{aligned}$$

UMF
$$v_{m} = \frac{1}{4\pi} \int_{0}^{2\pi} \int_{0}^{r_{t}} b q_{1}q_{2} r dr dv$$

$$v_{m} = \frac{1}{4\pi} \int_{0}^{2\pi} \int_{0}^{r_{t}} b q_{1}q_{3} r dr d\psi$$

$$q_{1} = (x - r \cos \psi) \sin \beta \sin \psi - (y - r \sin \psi) \sin \beta \cos \psi + z \cos \beta$$

$$q_2 = g_m \left(-\frac{\cos \phi}{s^3} - \frac{mn\Omega}{cs^2} \sin \phi \right) + h_m \left(\frac{\sin \phi}{s^3} - \frac{mn\Omega}{cs^2} \cos \phi \right)$$

$$q_{3} = g_{m} \left(-\frac{\sin \phi}{s3} + \frac{m n \Omega}{c s^{2}} \cos \phi \right) + h_{m} \left(-\frac{\cos \phi}{s3} - \frac{m n \Omega}{c s^{2}} \sin \phi \right)$$

$$\phi = m n \Omega \left(\frac{\psi}{\Omega} + \frac{s}{c} \right)$$

GMAR
$$\overline{g_m}(r, \psi) = \frac{n}{\pi b} \int_{-\infty/2r}^{\infty/2r} \overline{t}(r, \psi) \cos mn \psi d\psi$$

HMAR
$$\vec{h}_{m}(r, \psi) = \frac{n}{*b} \int_{-a/2r}^{a/2r} \vec{l}(r, \psi) \sin mn\psi \ d\psi$$

s
$$s = [(x - r\cos\psi)^2 + (y - r\sin\psi)^2 + z^2]^{\frac{1}{2}}$$

Program Listing

The listing for the complete noise prediction deck is contained in Figures 5 through 38. Figure titles correspond to the program or subroutine contained in the figure.

Limitations of the Program

Some aspects of the rotational noise prediction program limit its immediate operation by new users. The direct-access storage drums are called 28, 29, and 30 by the program and the NTRAN routine. It probably will be necessary to change these call numbers to match those used on the UNIVAC 1108 system.

Some additional changes will be required in the programmed equations if the rotor blades being studied differ from those of the NH-3A described in Volume I of this report. In particular, the span stations for which input pressure data are available are assumed to be 40%, 75%, 85%, 95%, and 98% of the radius (BLADEL). The program further assumes that the input chord stations or transducer locations are at 4.2%, 15.8%, 30%, 60%, and 91% chord (AA). In addition, the lifting surface of the blade is assumed to consist of the outer 80.1% of span. Changes in the chord locations will affect the interpolation routine used to calculate GMAR and HMAR, while changes to the span will affect the interpolation used to calculate GMARI and HMARI. These changes are not difficult to make once the programmer is familiar with the deck.

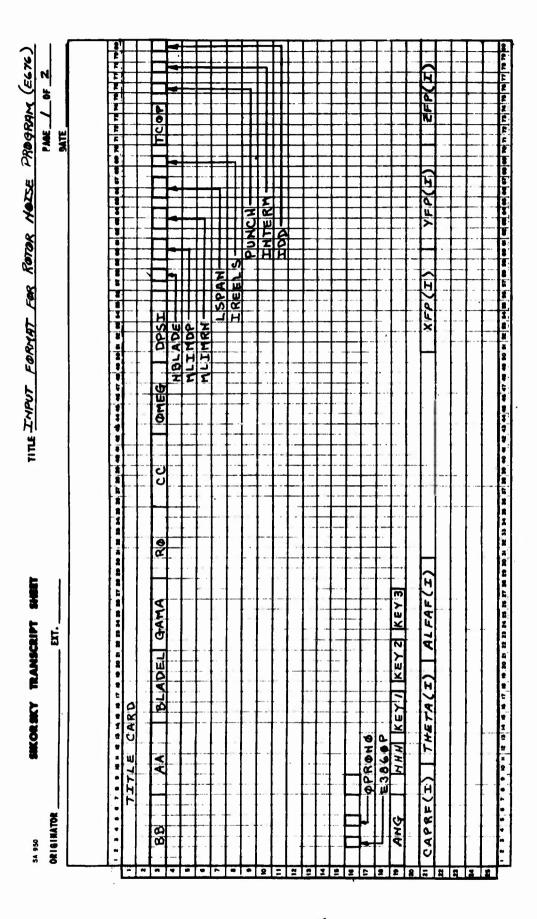


Figure 1. Sample Input, Symbolic.

BURST MO. SERBURST BURST		E E E E E E E E E E E E E E E E E E E			PATICS EDGE	AND 7	10	LONGITU LONGITU ADE ROO	DET PUT	# # # # # # # # # # # # # # # # # # #	GE THE	PECTIVEL	ELY)
BURST MO. = IIBURST BURST MO. = IIBURST BLADE PITCH MARMONICS OIFFERENTIAL PRESSURE COSINE CHERTICIENTS COSINE COEFFICIENTS SINE COEFFICIENTS SINE COEFFICIENTS SINE COEFFICIENTS SINE COEFFICIENTS		E E E E E E E E E E E E E E E E E E E	#		PATCS	AND 7	1	LONGITU 6 CONGITU CONGITU ADE ROG	DE NA	2 4 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	GE THE	2 S S S S S S S S S S S S S S S S S S S	ELY)
BURST HO. = INGURST BLADE PITCW WARMONICS OFFERENTEAL PRESSURE (MEASURING FROM THE LE. COSINE COEFFICIENTS CMESTAL COEFFICIENTS SINE COEFFICIENTS SINE COEFFICIENTS SINE COEFFICIENTS SINE COEFFICIENTS SULTAN SW(2,54,14)		ERENT CAN THE CONTRACT	7		PMICS PAICS	AND 7	CTIVE PU	LONGET O	DEWALL	A A A A A A A A A A A A A A A A A A A	GF TE	PECTIV S SPA	WS.
BURST WO. = IDOURST *** ROTOR WOISE PUNCHED GUTPUT *** BLADE PITCH WARMONICS COLLECTIVE, LONGITUDINAL, LATERAL COSINE CHERICAL PRESSURE HARMONICS FOR SCHOOL OF FACTOR FT IN COSINE CHERICAL STATES COSINE COEFFICIENTS SIME COEFFICIENTS	N 0	THE PLANT OF THE PARTY OF THE P				AND 7	CONFRO	LONGITU STAITED 6	DEMALL POT RESIDE	# # # # # # # # # # # # # # # # # # #	GE THE	PECTIV S SPA	WS.
BLADE PITCH HARMONICS BLADE PITCH HARMONICS COLLECTIVE, LONGITUDINAL, LATERAL DIFFERENTIAL PRESSURE WARMONICS FOR SCHOOL STATERAL COLLECTIVE, LONGING AT EACH OF THE BLADE AND THE BLADE ROOT RESPECTIVELY COSINE COEFFICIENTS CMESTAL COEFFICIENTS CMESTAL COEFFICIENTS CMESTAL COEFFICIENTS CMESTAL COEFFICIENTS CMESTAL COEFFICIENTS	0 478 0 478	ERENT CO	E A E E			PORKEC AND	TI VE	LONGITU STATIO ADE ROO	DTHALL MS AT	LATER EACH ECTIV	GE THE	PECTITY 5 SPA	ELY)
BLADE PITCH WARMWARCS BLADE PITCH WARMWICS TO COLLECTIVE, LANGER LEADING ENGIT UDING AT EACH OF STAND THE BLADE ROOT RESPECTIVELY THE COEFFICIENTS TWE COEFFICIENTS SIME COEFFICIENTS SWITH I SWITH SW	84.99	E PLING P	E E E			AMD 7	CON PRO	LONGITU STAITE ADE ROO	DINALL AT RES	LATER EACH ECTIV	GF TIE	PECTIV 5 SPA	(ELY)
DIFFERENTIAL PRESSURE HARMONICS FOR SCHOOL ANGERLALARALARALALARALALARALALARALALARALALARALALARALALARALALARALALARALALARALARALALARALALARALALARALALARALALARALALARALALARALARALALARALALARALALARALALARALALARALALARALALARALALARALALARALALARALALARALALARALALARALALARA	100	ERENT TAL	7			FOR S AND	CHORD	LOMGITU STAITIO ADE ROO	DYS AT	LATER EACH ECTIV	GETHE	PECTIV 5 SPA	(WS
DIFFERENTIAL PRESSURE HARMONICS FOR SCHORD TWE BLADE ROOT RESPECTIVELY WEASURING FROM THE LEADING EDGE AND TWE BLADE ROOT RESPECTIVELY SPAN CHORD STEADY = CH(I, SH,IH) COSINE COEFFICIENTS SINE COEFFICIENTS SINE COEFFICIENTS SINE COEFFICIENTS SINE COEFFICIENTS	1	SURING FR	E S C K K K K K K K K K K K K K K K K K K			AND 7	TIVE OL	LONGITUS STAITION ADE ROO	DEMAL.	LATER EACH ECTIV	94L RES 9F 7'E 1ELY).	PECTIV 5 SPA	ELY)
DIFFERENTIAL PRESSURE WARMONICS FOR SCHORD STATIONS AT EACH OF SCHORD STATIONS AT EACH OF SCHORD STATIONS AT EACH OF SCHORD TWE GLADS ROOT RESPECTIVELY SPAN CHORD - 5N STEADY = CH(!, 5N,IM) COSINE COEFFICIENTS CH(!, 5N,IM) SINE COEFF	1) 1.6	SURING FR	ESSUR 7%E	W W		FOR S	CHORD THE BL	A DE ROO	MS AT	EACH	0F 7"E	2 8 P	WS.
DIFFERENTANC PRESSURE HARMONICS FOR SCHOOL STATIONS AT EACH OF THE SURENTANC PROME THE LEADING EDGE AND THE BUADE ROOT RESPECTIVELY). SPAN CHORD STEADY = CH(!, SN,IH) SAMINANC COEFFICEENTS	7744	SURTING PR	ES3UR 7/1/5	T W	الإلا	AND		1 12	MS AT	EACH PECTIV	OF THE	W	WS
COSTME COEFFICIENTS STATE COEFFICIENTS		SURING FR	74E	Li)	} E09E	AND		140	IT RES	PECTIV	/ELY).	<u> </u>	
SPAM CHORD STEADY = CH(1, SH, EK) COSINE COEFFICIENTS CH(3, SH, EK) CM(2, SW, ZK) CH(3, SH, ZW)		4	MS										
SPAN CHORD STEADY= COSINE COEFFICIENTS CME, SWIZN, CH(3, SN, EN) SINE COEFFICIENTS SW(, SN, EN) SW(2, SN, EN)		4	NS	-					l	-			
COSTME COEFFICIENTS CMESTYLE COEFFICIENTS CMESTYLE COEFFICIENTS SINE COEFFICIENTS SMUTH COEFFICIENTS	-									-			
COSINE COEFFICIENTS CME, 34, 24, 24, 34, 44, 54, 54, 54, 54, 54, 54, 54, 54, 5	SPAM			STEAL		H(1,5h	Y, I'						
COSINE COEFFICIENTS CME, SW, ZN, ZN, ZN, ZN, SINE COEFFICIENTS SW(, SN, IN) SW(2, SN, IN)									ļ				
CM(Z, SW, ZM, CM(3, SM, ZW) SINE COEFFICIENTS SM(1, SM, ZM, ZM)	4COST		CIENTS						-				
CM(S) SW. ZW. ZW. ZW. S.	1	-						130					
SIWE COEFF	ew(Z,	34,2K) CH(3	コンシュン	6								-	
SINE COEFF	,				-								
SINE COEFF			-			10							
SM(J3M, ±N)			ENTS	100		0						7	
SM(,3%, ± v)					-		S						
	1 SW(1,3	~	(NZ/YS'	• • •						-			
	2												
	9		-										
	•												
	2												

Figure 1. Sample Input, Symbolic - Concluded.

							_	Ed.		i																		1	İ
																										DATE			
		1		9			8	8 8	1	2 2	2	· · · · · · · · · · · · · · · · · · ·	*	1		2 2 2		* 60	3 9		2	2 2	3	*** * * * * * * * * * * * * * * * * *	8 5 7	8 8 70 71	1 TE 75 74 75 76 77 76 79,00	2 2	1 5
17-5	15	9/	165KT	MOY		WING	7 4		DI	40	8	ADING-BHARMONICS	E.	IC		7	1(R. PSI	ij											
					-	-	1					İ									-							-	
2	0		/8:	2	372		0	0.0	0134	*	7	72.0	-	13	13040.0	0		204.0	0	2.5	-	5	Ø	4	20	0	CARD	2	z
4 N	Σ	10								 		-	-				1								-				1
	21.5	7.7	+	Ö	-	0	8		-				-		1						-								
124	5.0		1	69.9	6		-23	•	20				1			2			-	-76800	00	0	30	00	0	+	7320	0.0	
6///	7.0		,	166.	0		-	0	.33			-			-					120	12000.0	0	30	3000.0	0	'	7296.0	0.0	
1111	4.0		1/	164.	2		-33	3	.07				-		-					108	10800.0	0	30	3000.0	0	'	7296.0	0.0	
1035	5.0		/	162.2	2		-35	5.	76.					-						-96	0.0096-	0	30	3000.0	٥	,		0.9	
	0		~	160.	9		1	٠ •	82		-				700					-,84	-8400.0	٥	30	3000.0	0	′.	-7296.0	6.0	
890			1	/157.	0		1	+	80.											- 7200.0	00	0	30	3000.0	0	'	-7296.0	0	
12 82			1	3			-47	1	40				11							- 6000.0	00	0	30	3000.0	0	-	0.9674-	0.9	
	0		\$	146.0			- 52	2	0				-							1.6	-1800.0	0	30	3000.0	0		-7296.0	0	
				140.2	7		3	57.	20	-			-		side a					-3600.0	00	٥	30	3000.0	٥		-7296.0	0.9	
18 687.	9.		`	/28.	7		7	25	. 23						-1					- 2400.0	00	0	30	3000.	٥		7296.0	0	
2													-																1
12																													
9.	-							-						٠.															
•		-																							-				
				-						-															-				1
1.8			- 0				-																						
- 4		-					_ :		=																				
									-																		2		
		_							-	=																			
	-	-				Ī																							L

Figure 2. Sample Input, Numeric.

### ROTOR HOLSE PUNCHED OUTPUT ### ### STEADY ### SOOTO OUTPUT ### ### STEADY ### SOOTO OUTPUT ### ### STEADY ### SOOTO OUTPUT ### ### STEADY ### SOOTO OUTPUT ### ### STEADY ### SOOTO OUTPUT ### ### STEADY ### SOOTO OUTPUT ### ### STEADY ### SOOTO OUTPUT ### #### STEADY ### SOOTO OUTPUT ### #### STEADY ### SOOTO OUTPUT ### #### STEADY ### SOOTO OUTPUT #### ###############################	
######################################	
### ### ### ### ### ### ##############	1 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
UNIST MO. 13 *** ReteR HOUSE PUNCHED BUTPUT *** UNIST MO. 13 *** ReteR HOUSE PUNCHED BUTPUT *** UNIST MO. 13 *** RetER HOUSE RETERENT *** UNIST MO. 14 *** UNIST MO. 14 *** UNIST MO. 15 *** UNIST MO. 15 *** UNIST MO. 15 *** UNIST CONTROL FROM THE LEADER SCHOOL STATEOUS AT EACH OF SPANNING RESPECTIVE LANDER RIGHT RESPECTIVE LANDER RIGHT RESPECTIVE LANDER RIGHT RESPECTIVE LANDER RIGHT RESPECTIVE LANDER RIGHT RESPECTIVE LANDER RIGHT RESPECTIVE LANDER RIGHT RESPECTIVE LANDER RIGHT RESPECTIVE LANDER RIGHT RESPECTIVE LANDER RIGHT RESPECTIVE LANDER RIGHT RESPECTIVE LANDER RIGHT RESPECTIVE LANDER RIGHT RESPECTIVE LANDER RIGHT RESPECTIVE LANDER RIGHT RESPECTIVE LANDER RIGHT RESPECTIVE LANDER RIGHT RESPECTIVE RESPECTIVE RESPECTIVE RESPECTIVE RESPECTIVE RESPECTIVE RESPECTIVE RESPEC	
94.40E PTTCH HARMONICS 9.5150 1.5750 1.7878 9.5754 9.5762 1.57550 1.7867 9.5754 1.7867 9.7546 1.7867 9.7546 9.7556 9.7556 9.7567 9.756	MO. =13 WHY ROTOR HOTSE PUNCHED BUTPUT
1.5/50 // 78/8 9./544 COLLECTIVE, LONGITUDINAL, LATERAL RESPECT DIFFERENTIAL PRES UNE MARMONICS FOR S CHORD STATIONS 47 EACH OF S SPANN (MESPECTIVE, LONGING PROM THE STEADS ATTIONS 47 EACH OF S SPANN (MESPECTIVE, CONGINE BY STEADY F / 0363+00 10-2146 CONFIGURE STEADY F / 0363+00 10-2146 CONFIGURE STEADY F / 0363+00 10-2146 CONFIGURE STEADY F / 0363+00 10-2146 CONFIGURE STEADY F / 0363+00 10-2146 CONFIGURE STEADY F / 0364+00 10-3146 CONFIGURE STEADY F / 0364+00 10-3146 CONFIGURE STEADY F / 0358+00 10-3146 CONFIGURE STEADY F / 00/6-07 10-00	PITCH HARMONICS
DIFFERENTIAL PRES WE MARRONICS FOR S CHORD STATIONS 47 EACH OF S PANNO PERSONAL PRESSORY OF S PANNO PERSONAL PRESSORY OF S PANNO PERSONAL PRESSORY OF S PANNO PERSONAL PRESSORY OF S PANNO PERSONAL PRESSORY OF S PANNO PERSONAL PRESENTANCE WE PLADE RIGHT S PANNO PERSONAL PRESENTANCE WE PERSONAL PRESSORY OF S PANNO PERSONAL PRESENTANCE WE PERSONAL PRESSORY OF S PANNO PERSONAL PRESENTANCE WE PERSONAL PRESSORY OF S PANNO PERSONAL PRESSOR OF PERSONAL PRESENTANCE PERSONAL PRESENTANCE PERSONAL PRESENTANCE PERSONAL PRESENTANCE PERSONAL PRESENTANCE PERSONAL PRESENTANCE PERSONAL PRESENTANCE PERSONAL PRESENTANCE PERSONAL PRESENTANCE PERSONAL PRESENTANCE PERSONAL PRESENTANCE PERSONAL PROPERTY	0 1.7878 9.1546
MEMS WATMY FROM THE MADEN EDGE AND THE ELABE KINT RESPECTANCELY CHORD CHORD STEADY=1.0363+00 STEADY=1.0363+00 STEADY=1.0363+00 STEADY=1.0363+00 STEADY=1.0363+00 STEADY=1.0363+00 STEADY=1.0363+00 STEADY=1.0329-01-1.1329-01-1.0611-01-5.3502-02 O455-02 STAE COEFFICIENTS STEADY=5.7707-01 STEADY=1.0494-01 STEADY=5.7707-01 STEADY=1.0494-01 STEADY=2.3444-01 STEADY=2.0494-01 STEADY=2.3444-01 STEADY=2.3949-02-5.2198-02-1.2333-02-5.7960-04 STEADY=2.3949-02 STEADY=2.3949-02-1.2333-02-5.7960-04 STAE COEFFICIENTS STEADY=2.23949-02-1.2333-02-5.7960-04 STAE COEFFICIENTS STEADY=4.90/6-07 STAE COEFFICIENTS STEADY=4.90/6-07 STAE COEFFICIENTS STEADY=4.90/6-07	PRESENTE HARMONIZOS FOR S CHORD STATIONS AT EACH OF
SPAN / CMORP / CMORP / STEADY=1.0363+00 10 SING CONFIGURENTS 5. N 133-01 5.9133-01 2.4036-01-1.1329-01-1.0611/-01-5.3502-02 1.0455-02 5. N 263-01 5.9133-01 5.7926-01 2.5240-01 1.2364-01 2.5328-02 4.5821-02 5. N 266-01-6.8349-01 5.7926-01 2.5240-01 1.2364-01 2.5328-02 4.5821-02 5. N 266-01-6.8349-01 1.3409-01-5.6017-02-7.3457-02-2.3293-02 7.8033-03 5. N 266-01-3.134-01 2.2282-01 1.3558-01 5.6567-02 9.7851-03 2.8522-02 5. N 269-01 3.7734-01 2.2282-01 1.3558-01 5.6567-02 9.7851-03 2.8522-02 5. N 269-01 3.0031-01 4.9981-02-2.3949-02 1.3377-02 1.3377-02 1.3645-02 5. N 2626-01-3.0031-01 9.3589-02 5.8539-02 1.3377-02 1.3645-02 5. N 2626-01-3.0031-01 9.3589-02 2.8389-02 1.3377-02 1.3645-02	SURTING FROM THE LEADING EDGE AND THE BLADE RIGHT RESPECTIVE LY
20 S Z Z Z 2 0 DE FELCIENTS 9. 82 63 - 01 5.9 13 3-07 2.4036-07-1.1329-07-1.0617-01-5.3502-02 7.0455-02 5. 74 6 CDE FELCIENTS 7. 76 56-57-6.8 249-01 5.7926-01 2.5240-01 7.2364-01 2.5328-02 4.5827-02 5. 77 6 56-57-6.8 249-01 5.7926-01 2.5240-01 7.2364-01 2.5328-02 4.5827-02 6. 5 Z ME COEFFICIENTS 5. 10 75-01-3.7739-01 2.2282-01 1.3558-01 5.657-02-2.3293-02 7.8033-03 5. 11 75-01-3.7739-01 2.2282-01 1.3558-01 5.657-02-2.3293-02 7.8033-03 5. 11 75-01-3.7739-01 2.2282-01 1.3558-01 5.657-02 9.7857-03 2.8522-02 5. 11 75-01-3.7739-01 4.9981-02-2.3969-02-7.2333-02-5.7960-04 5. 12 6526-01-3.0031-01 9.3589-02 2.8389-02 7.3377-02 7.3645-02 5. 6526-01-3.0031-01 9.3589-02 2.8389-02 7.3377-02 7.3645-02 5. 6526-01-3.0031-01 9.3589-02 2.8389-02 7.3377-02 7.3645-02	1 CMORD 1 STEADY=1.0363+00
9.8263-01 5.913-07 2.4036-01-1.1329-01-1.0611-01-5.3502-02 1.0455-02 5.146 CDEFFICIENTS 7.7656-01-6.8249-01 5.7926-01 2.5240-01 1.2384-01 2.5328-02 4.5821-02 5.994 1 CHORD 2 5.1175-01-3.7734-01 2.2282-01 1.3558-01 5.657-02-2.3293-02 7.8033-03 5.1175-01-3.7734-01 2.2282-01 1.3558-01 5.657-02 9.7851-03 2.8522-02 5.1175-01-3.7734-01 2.2282-01 1.3558-01 5.657-02 9.7851-03 2.8522-02 5.1269-01 1.7189-01 4.9981-02-2.3969-02-1.2333-02-3.7960-04 5.6526-01-3.0031-01 9.3589-02 5.8573-02 1.3377-02 1.3645-02 5.6526-01-3.0031-01 9.3589-02 5.8389-02 1.3377-02 1.3645-02 5.6526-01-3.0031-01 9.3589-02 5.8389-02 1.3377-02 1.3645-02	ME COEFFICIENTS
SIME CDEFFICIE WTS 7.76.56-C1-6.8 449-01 5.7926-01 1.2384-01 2.5328-02 4.5821-02 SPAN 1 CHORD 2 4.8362-01 2.6494-01 1.3409-01-5.6017-02-7.3457-02-2.3293-02 7.8033-03 5.1175-01-3.7734-01 2.2282-01 1.3558-01 5.6567-02 9.7851-03 2.8522-02 SPAN 1 CHORD 3 57EADY=2.3444-01 COSTME COMPFICIENTS 5.1175-01-3.7734-01 2.2282-01 1.3558-01 5.6567-02 9.7851-03 2.8522-02 STAE COMPFICIENTS 5.6699-01 1.7789-01 4.9981-02-2.3969-02-7.2333-02-5.7960-04 STAE COMPFICIENTS 5.6656-01-3.0031-01 9.3589-02 5.8273-02 2.8389-02 1.3377-02 1.3645-02 SPAN 1 CHORD 4 576ADY=4.9016-07	.8263-01 5.9133-01 2.
7.7656-C1-6.8749-01 5.7926-01 2.5240-01 1.2364-01 2.5328-02 4.5821-02 SPAN 1 CHORD 2 10.5 THE COFFETCE FATS 4.8362-01 2.2694-01 1.3409-01-5.6017-02-7.3457-02-2.3293-02 7.8033-03 5.1175-01-3.7734-01 2.2282-01 1.3558-01 5.6567-02 9.7851-03 2.8522-02 SPAN 1 CHORD 3 57EADY=2.3444-01 COSTME COFFETCE FATS -3.6099-01 1.7189-01 4.9981-02-2.3949-02-7.2333-02-5.7960-04 STAE COFFETCE FATS -3.6099-01 1.3377-02 3.8589-02 2.8389-02 1.3377-02 3.3458-02 SPAN 1 CHORD 4 STEADY=-4.9016-07	CDEFFICIENTS
SPAN 1 CHORD 2 COSTNE COEFFICHENTS -4. B362-01 2.6994-01 1.3409-01-5.6017-02-7.3457-02-2.3293-02 7.8033-03 SIME COEFFICIENTS STEADY=2.3444-01 CHORD 3 57EADY=2.3444-01 CHORD 3 57EADY=2.3944-01 STEADY=2.3944-02 STEADY=2.3949-02 5.8589-02 7.8033-02-5.7960-04 STEADY=3.6099-01 1.3333-02-5.37960-04 STAKE COFFFICIENTS STAKE COFFFICIENTS STEADY=4.9016-02 5.8389-02 1.3377-02 1.3645-02 SPAN 1 CHORD 4 57EADY=4.9016-07	5.7926-01 2.5240-01 1.2384-01 2.5328-02
COSTME COFFICIENTS -4.8362-01 2.694-01 1.3409-01-S.6017-02-7.3457-02-2.3293-02 7.8033-03 -51ME COFFICEENTS -5.1175-01-3.7734-01 2.2282-01 1.3558-01 5.657-02 9.7851-03 2.8522-02 -5.1175-01-3.7734-01 2.2282-01 1.3558-01 5.657-02 9.7851-03 2.8522-02 -5.6099-01 1.7189-01 4.9981-02-2.3969-02-7.2333-02-5.7960-04 -5.6099-01 1.7189-01 4.9981-02-2.3969-02 1.3377-02 1.3645-02 -5.6526-01-3.0031-01 9.3589-02 5.8573-02 2.8389-02 1.3377-02 1.3645-02 -5.6526-01-3.0031-01 9.3589-02 5.8573-02 2.8389-02 1.3377-02 1.3645-02	1 CHORD 2 STEADY . S. 7707 - 0/
-4.8362-01 2.694-01 1.3409-01-5.6017-02-7.3457-02-2.3293-02 7.8033-03 SIME CORFFICHENTS STEADY=201 1.3558-01 5.6567-02 9.7851-03 2.8522-02 SPAN 1 CHORD 3 57EADY=2.3444-01 COSTME CORFFICHENTS -3.6099-01 1.7189-01 4.9981-02-2.3969-02-7.2333-02-5.7960-04 STAE CORFFICHENTS 2.6526-01-3.0031-01 9.3589-02 5.8389-02 1.3377-02 1.3645-02 SPAN 1 CHORD 4 57EADY=4.9076-07	COEFFICEENTS
51 WE COEFFICIENTS 5. 11 75-01-3.7734-01 2.2282-01 1.3558-01 5.6567-02 9.7851-03 2.8522-02 5. 11 75-01-3.7734-01 2.2282-01 1.3558-01 5.6567-02 9.7851-03 2.8522-02 5. 11 75-01-3.7734-01 2.2282-01 1.35587-02 2.8389-02 1.337-02 1.3645-02 5. 6526-01-3.0031-01 9.3589-02 5.8273-02 2.8389-02 1.3377-02 1.3645-02 5. 6526-01-3.0031-01 9.3589-02 5.8273-02 2.8389-02 1.3377-02 1.3645-02 5. 6526-01-3.0031-01 9.3589-02 5.8673-02 2.8389-02 1.3377-02 1.3645-02	1.3409-01-5.6017-02-7.3457-02-2.3293-02
5.1175-01-3.7734-01 2.2282-01 1.3558-01 5.6567-02 9.7851-03 2.8522-02 5PGH 1 CHORD 3 5TEADY=2.3444-01 COSTHE CORFETCIENTS -3.6099-01 1.7789-01 4.9981-02-2.3969-02-5.2198-02-1.2333-02-5.7960-04 5THE CORFETUIENTS 2.6526-01-3.0031-01 9.3589-02 5.8273-02 2.8389-02 1.3377-02 1.3645-02 SPAH 1 CHORD 4 5TEADY=-4.9016-07	COEFFICTEMTS
5PAH 1 CHORD 3 STEADY=Z.3444-01 COSTHE CORFETCIENTS -3.6099-01 /.7/89-01 4.9981-02-2.3949-02-5.2/98-02-1.2333-02-5.7960-04 STHE CORFETCIENTS 2.6526-01-3.0031-01 9.3589-02 5.8273-02 2.8389-02 /.3377-02 /.3645-02 SPAH 1 CHORD 4 STEADY=-4.90/6-07	2.2282-01 1.3558-01 5.6567-62
COSTME CORFETCIFENTS -3.6099-01 /.7/89-01 4.9981-02-2.3949-02-5.2198-02-1.2333-02-5.7940-04 SIME CORFETCIENTS 2.6526-01-3.0031-01 9.3589-02 5.8273-02 2.8389-02 1.3377-02 1.345-02 SPAN 1 CHORD 4 STEADY=-4.90/6-02	1 CHORD 3 STEADY = 2.3444-01
-3.6099-01 1.7189-01 4.9981-02-2.3949-02-5.2198-02-1.2333-02-5.7940-04 SIME COFFETCIENTS 2.6526-01-3.0031-01 9.3589-02 5.8273-02 2.8389-02 1.3377-02 1.3645-02 SPAN 1 CHORD 4 STEADY=-4.90/6-02	HE CORFETCIENTS
STAE COFFFICIENTS 2.6526-01-3.0031-01 9.3589-02 5.8273-02 2.8389-02 1.3377-02 1.3645-02 SPAN 1 CHORD 4 STEADY=-4.90/6-02	1.7/89-01 4.9981-02-2.3969-02-5.2198-02-1.2333-02-
2.6526-01-3.0031-01 9.3589-02 5.8273-02 2.8389-02 1.3377-02 1.3645-02 SPAH 1 CHORD 4 STEADY=-4.90/6-02	COEFFICIENTS
SPAN 1 CHORD 4 STEADY=-4,90/6-07	526-01-3.0031-01 9.3589-02 5.8273-02 2.8389-02 1.3377-02
	1 CHORD 4 STEADY = - 4.90/6-02
POSINE COEFFICIENTS	COEFFICIENTS
1-01 8.3637-02 1.9119-02-8.1379-03-1.9951-02 7.0415-04-3.1862-03	-01 8.3637-02 1.9119-02-8.1379-03-1.9951-02
1	
3.5763-02-1.2231-01 2.6333-02 2.9186-02 1.0332-02-4.3339-03 8.9812-04-6.	2.6333-02 2.9/86-02

Figure 2. Sample Input, Numeric - Continued.

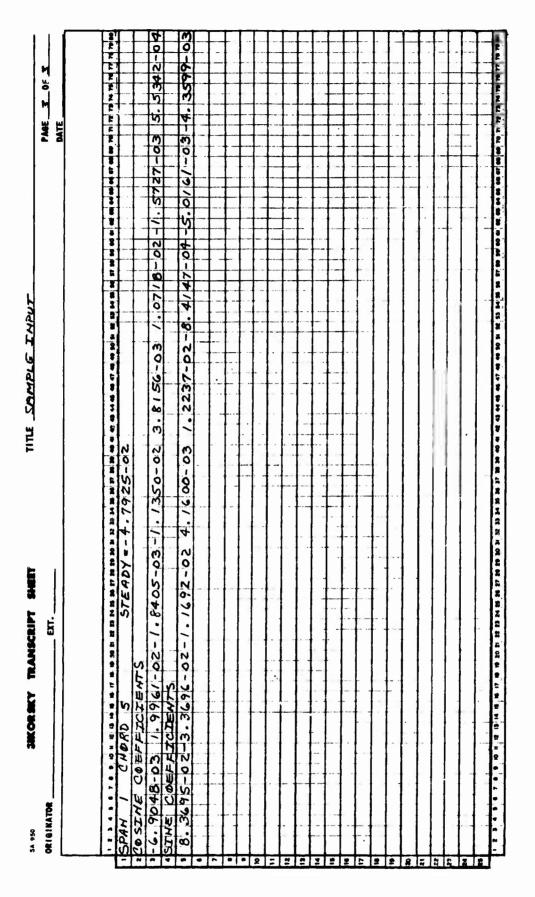


Figure 2. Sample Input, Numeric - Concluded.

													0 KEY32 0													
				•	E CARD	TION	2 11	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2			!		O KEYZE	INTS	Z (IN)	7320+04	7296+04	-,7296+04	-,7296+04	-,7296+04	-, 7296+04	7296+04	-,7296+04	-,7224+04	7224+04	7224+04
1102767	= .7400+02	.1304+05	-2040+03	= .2500+01	NOILLON	PRESSURE HARMONIC PUNCH, OPTION	INTERMEDIATE OUTPUT OPTION			•	1		S = 16 KEY1=	ROTOR NOISE FIELD POINTS	Y (IN)	\$0000÷0*	. 3000+0+	*0+000°	3000+04	#0+000°	3000+0+	*0+000E*	*0+000°	#0+000°	*0+000€	3000+0¢
WING LOADING 16 HARMONICS LIRTPST 1102767	A. (IN)	(IN/SEC)	(Hell)	(066)	TAPE / CARD OPTION	PRESSURE HARI	INTERMEDIATE			≻ Ⅱ	» #	=14	NO. OF AIR LOAD HARMONICS =	ROTOR	X CIN)	-,1680+05	1200+05	9600+04	100000	6000+04	+0+000+	3600+04	2400+04	*0+00*2	*0+0009*	*0+0096
6 - 16 HARMON	ZERO THIST BLADE STA.	SPEED OF SOUND	ROTOR ROT. SPEED	AZIMUTH INCREMENT			,	2		URE PULSE)	PULSE)		NO. OF AIR		£	-	N F) <i>æ</i>	IO 4) r	••	Φ,	2:	15	2	14
W WING TOKOTH	ZERO	SPEED	ROTOR	AZIMUT	11	CYCLES = 16	0,	= 20	н	CONST. PRESS	URED PRESSURE	ì) = 2.5000	ķ	ALPHA (DEG)	-,2320+02	3033+02	3597+02	-,3928+02	-,4740+02	5218+02	5728+02	-,6223+02	-,6200+02	4710+02	3570+02
S-61F TESKT LOW	= .2000+01	= ,1820+02	= .3720+03	.1340-01		SENT PRESSURE CYCLES	SOI	STATIONS		S (THEORETICAL	PROGRAM : SEAS		IN E386 (LIG.	E386 FIELD POINTS	THETA (DEG)	.1699+03	.1660+03	.1622+03	1603+03	1534+03	.1480+03	.1402+03	1287+03	.5130+02	.2660+02	.1740+02
	SS (IN)	(IN)	(N1)	BLADE TWIST RATE (DEG/IN)	LDE'S	NO. OF HARMONICS TO REPRESENT	NO. OF ROTOR NOISE HARMONICS	NO. OF INTERPOLATED SPAN STATE	TAPE REELS	OPTION TO USE PROGRAM E386 (THEORETICAL CONST. PRESSURE PULSE)	OPTÍON TO USE ROTOR NOISE PROGRAM ; MEASURED PRESSURE PULSE;	POINTS	INCR. OF INTEGRAȚION USED ÎN E386 (LIG.)	£36	R (FT)	.1545+04	.1197+04	1035+04	.9600+03	.8260+03	.7690+03	.7230+03	.6870+03	.6820+03	.6220+03	.1031+04
	BLADE THICKNESS (IN)	BLADE CHORD	BLADE LENGTH	BLADE THIST H	NUMBER OF BLADES	NO. OF HARMON	NO. OF ROTOR	NO. OF INTER	TOTAL NO. OF TAPE REELS	OPTION TO USE	OPTION TO USE	NO FOF FIELD POINTS	INCR. OF INTE		e e	-	N F) <i>a</i> t	u 4	۰,	80	6	01:	12	13	74

Figure 3. Sample Output.

CHORD STATION 1

SPAN STATION 1

3,7674-01 1,7674-01 1,2764-01 2,7936-01 2,6391+00 1,6639-00	7.4450-01 3.0265-02 9.1600-01 1.6254-00 1.4267-01 7.0127-01 -1.3596-02 -5.5169-02 1.1028-03 7.6179-03	
1.14 + 00 1.14 + 00	7.4682-01 5.4682-01 6.458-01 1.7878-01 1.7878-01 1.5272-00 7.658-01 2.4708-01 2.4708-01 1.3508-01 1.3508-01 1.3508-01	6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
6.86.7601 9.10.8601 9.10.8601 9.10.8601 9.10.8600 1.10.8600 1.10.86900 1.10.86900 1.10.86900 1.10.86900 1.10.86900 1.10.86900 1.10.86900 1.10.86900 1.10.86900 1.10.86900 1.10.86900 1.10.86900 1.10.86900 1.10.86900 1.10.86900 1.10.86900 1.10.86900 1.10.86900	7.3159-01 7.3159-01 7.3508-02 7.3508-02 1.7271-00 1.608-00 8.2573-01 2.1674-01 2.1674-01 1.648-02 -2.1674-01 9.0767-02	13.998.5999.5999.5999.5999.5999.5999.5999
2.5531-01 7.1393-01 7.1393-01 7.1393-01 3.5237-00 1.5532+00 1.0985-01 1.0985-01 1.1585-01 1.1585-01	7.0421-01 -3.7642-01 -3.7952-02 -3.7952-02 1.6418+00 1.6724-00 8.7974-01 2.9111-02 -4.3769-02 -2.3228-02 1.9328-02 1.9328-02	1.0502-01 2.0464-02 2.0464-02 2.0464-02 3.0464-01 1.0392-01 5.0362-01 1.0362-01 1.0362-01 1.0362-01 1.0626-01 1.0626-01
9,5082-01 5,2526-01 5,2526-01 3,4851-00 1,3861-00 1,388-01 1,3090-01 1,388-01 1,588-01 2,888-01 2,888-01 2,9971-02	6.6599-01 -3.4269-02 -5.261-01 1.5372-00 1.7160+00 9.3056-01 2.9594-02 -2.9594-02 -2.9594-02 -2.9594-02	1. 7961-01 2.2460-01 2.2460-01 2.0166-01 1.0126-01 1.0126-01 1.0126-01 1.0098-01 1.10098-01 2.5966-01
1.08648-00 2.7627-01 3.0438-00 3.64452-00 1.8249-00 1.6891-01 1.6891-01 3.2738-01 3.2738-01	5.7597-01 1.4598-02 1.4598-02 1.8520-00 1.8520-00 1.7820-00 2.7820-01 2.7820-01 2.7800-02 -2.080-02 1.3253-01	4.54747-01 4.542-02 2.2328-01 1.3596-01 1.0253400 1.0253400 1.02538-01 1.7265-01 -1.356-01 -1.4566-01 9.4500-01 9.4500-01
1.1969-01 1.29450-01 1.29450-01 3.40384-00 1.9450-01 1.9450-01 2.2436-01 1.7252-02 1.7255-03 4.2555-03	5.6492-01 6.2225-01 5.275-02 5.1276-02 1.33156-00 1.7597-00 1.7597-00 1.0467-00 1.0467-00 1.0457-01 1.0023-02 1.8028-02 1.8028-02 1.8028-02	8.8804-02 7.4258-02 7.4258-02 1.0258-03 1.0258-03 1.0257-03 1.0367-03 1.2560-03 1.2560-03 1.2560-03 1.2560-03 2.3734-02 2.5974-02
10-0891-6-7-00-8-6-6-7-6-7-6-7-6-7-6-7-6-7-6-7-6-7-6-7	11 5.0269-01 5.0269-01 5.0269-01 2.1959-01 1.1956+00 1.1956+00 1.7726+0	4 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
1.3696+00 1.3696+00 1.5696+00 3.3093+00 3.5226+00 3.5226+00 3.5126+00	CHORD 7.4.3257-(7.0358-01 1.4162-01 1.0956+00 1.75894+00 1.2155+00 5.7581-02 -4.6281-02 -5.1045-02 -5.1045-02 1.0071-01	CHORD ST 3,5325-02 1,1823-01 -3,7337-02 1,0208-01 1,0208-01 1,0208-01 2,9752-01 -6,1752-02 -1,3097-01 2,2706-02 4,4298-02
1.4179-00 2.1469-01 2.1469-01 3.21961-01 3.5124-00 3.55124-00 4.2249-00 4.2249-01 6.1915-02 9.1106-02 7.2341-03	SPAN STATION 1 2, 136-01 2, 1426-01 2, 1426-01 7,8274-02 1,0045+00 1,045-00 1,186+00 1,241-01 1,241-01 1,241-01 6,3624-02 6,5624-02 4,4653-02 9,9669-02	SPAN STATION 1 1,3159-03 -1,3159-03 -1,3159-03 4,018-00 1,018-01 1,018-01 3,423-01 -1,3124-01 -1,3124-01 -1,0113-02 -1,0113-02 -1,0113-02 -1,0113-02

Figure 3. Sample Output - Continued.

1,4824-02 1,986-01 1,986-01 1,000-01 1,786-01 1,788-01 1,5178-01 1,5178-01 1,5178-02 1,5178-02 1,5178-02	13, 14, 16, 17, 18, 17, 18, 18, 18, 18, 18, 18, 18, 18, 18, 18	4,7852-00 3,0865-00 3,0865-01 4,5865-01 4,7822-00 3,9977-00 2,6892-00 2,6892-00 2,6892-00 2,6892-00 2,6892-00 2,6892-00 2,6892-00 2,6892-00 2,6892-00 2,6892-00	3,4764+00 3,0216+00 1,6696+00
-5.056-02 -6.056-01 -6.056-01 -6.056-01 -6.058-01 -6.056-02 -6.056-02 -6.056-02 -6.056-02	-3.500 -0.00	4,9446+00 4,7455-01 4,4268+00 4,4268+00 4,1468+00 2,6844+00 2,6844+00 2,0469+00 2,0469+00 3,7397+00	3.4925+00 3.1350+00 1.7712+00
	2.3.64199.02 2.4440.03 2.4440.03 2.31576.03 3.6590.02 1.36586.03 1.36586.03 1.3186.03 1.3186.03 1.3385.03 1.3385.03 1.3385.03	5.0775+00 3.0145+00 6.7725-01 4.2862-00 4.2913+00 4.2913+00 2.6822+00 2.6822+00 2.6822+00 3.6353+00 3.6363+00	3,4948+00 3,2280+00 1,9118+00
-6.1390-02 -2.9278-01 -2.9278-01 -3.9278-01 -3.928-01 -3.9382-01 -3.9382-01 -3.9382-01 -2.9911-02	-3.7944-02 -3.1964-02 -1.5240-02 -2.327-02 -9.327-02 -9.327-03 -9.637-03 -1.3534-01 -1.1159-01 -1.1159-01 -1.6550-02	5,1852+00 8,2812+00 8,8174-01 3,9894+00 4,9259+00 4,114+00 2,6877+00 2,5854+00 1,9294+00 2,556+00 3,529+00 4,6118+00	3,4822+00 3,2956+00 2,0703+00
-6.3209-02 -1.5441-01 -2.9132-01 -1.9145-01 1.0556-01 2.0556-01 2.0556-01 -1.7078-01 -1.7078-01 -2.2988-02 -4.7485-02	13.2050-01 14.2050-02 15.3069-02 16.3069-02 16.3069-02 16.3069-02 16.3069-02 17.2050-01 17.2050-01 17.2050-01 17.2050-01 17.2050-01	5.2707+00 3.5256+00 1.0735+00 3.5171-00 4.5171-00 4.507+00 2.7002+00 2.7002+00 2.2557+00 2.4002+00 3.4014+00 4.5283+00	3,4577+00 3,3386+00 2,2284+00
-8.4647-02 -2.6602-01 -2.6602-01 -2.6602-01 -3.9143-01 -5.197-02 -1.928-01 -1.928-01 -1.928-01 -1.958-01	-3.46.1059-02 -2.9627-02 -2.0936-02 -2.0936-02 -3.4828-02 -3.4828-02 -1.2838-01 -2.0336-01 -2.0336-01 -3.115-01 -3.7134-02	5.331+00 4.3531+00 4.3533+00 8.3066+00 4.7626+00 4.3524+00 2.7150+00 2.7150+00 2.7150+00 2.372+00 4.4256+00	3,4258+00 3,3641+00 2,3759+00
-6.5564-02 -7.2606-01 -7.2606-01 -7.2606-01 -7.266-01 -7.266-01 -7.7606-01 -7.7606-01 -7.7606-01 -7.7606-02 -7.7606-02 -7.7606-02	-4.185502 1.3.6274-02 12.6156-02 13.6196-02 13.6491-02 13.7911-02 13.761-01 11.9451-01 11.9451-01 11.9451-01 11.9451-01	5.3760+00 3.9727400 1.4342400 2.2338400 4.6313400 4.6313400 2.5263400 2.7265400 2.7265400 2.7265400 2.7265400 2.7265400 7.216843400 3.312843400 5.3166400	3,3902+00 3,3819+00 2,5117+00
-6.6039-02 -1.1442-01 -2.6351-01 -2.1774-01 2.0531-02 1.9270-01 1.4441-01 1.4441-01 -2.4935-02 -1.2969-01 -1.2969-01 -1.2969-01 -2.9907-02	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	57ATION 1 5.3880+00 1.6352+00 2.51694-01 1.5947+00 4.5193+00 4.5193+00 3.6265+00 2.7355+00 2.7355+00 2.7355+00 2.7355+00 2.7355+00 2.7356+00 2.7358+00 3.666+00 4.1814+00 5.1109+00	3.3519+00 3.4004+00 2.6405+00
-0.6987-02 -1.0177-01 -2.4738-01 -2.4187-01 -3.9917-03 -1.5802-01 -1.5802-01 -1.754-01 -1.754-01 -1.754-01 -1.3754-01 -1.3754-01 -2.1367-02	CHORD ST -*, 1627-02 -3, 5260-02 -2, 7466-02 2, 7200-02 5, 5078-02 -1, 2101-02 -1, 2101-02 -1, 174-02 -1, 174-02 -1, 174-02 -1, 174-02 -1, 174-02 -1, 174-02 -1, 174-02 -1, 174-02 -1, 174-03 -1, 174-	CHORD 5,3657+0 4,3999+00 1,8690+00 1,6690+00 1,6759+00 4,4570+00 3,7395+00 2,7409+00 2,7409+00 2,0323+00 2,0323+00 2,0323+00 4,0590+00 4,0590+00 4,0590+00 4,0590+00 4,0590+00 4,050+00 4,050+00 4,050+00 4,050+00 CHORD	3,3087+00 3,4240+00 2,7682+00
-8,8635-02 -2,2968-01 -2,5150-02 -2,5150-02 1,8713-01 1,9695-01 1,9695-01 1,1475-01 -1,484-01 -1,484-01 -1,5591-02 -6,5591-02	SPAN STATION 1 -4,0680-02 -3,4513-02 72,5598-03 2,5399-02 2,5399-02 2,5399-02 -7,1599-02 -7,1599-03 -1,0675-02 -1,0675-02 -1,0675-02 -1,0675-02 -1,0675-02 -1,0675-02 -1,055-02	5,3076+00 4,6015+00 2,1370+00 2,1370+00 2,1370+00 1,44659+00 4,6654+00 3,6603+00 2,7595+00 2,7595+00 2,137+00 2,137+00 2,146+00 3,9446+00 3,9446+00 3,9446+00 3,9446+00 3,9446+00 3,9446+00	3.2571+00 3.4513+00 2.6966+00

Figure 3. Sample Output - Continued.

1,9967+00 3,99867+00 3,99867+00 1,69867+00 1,6667+00 1,0620+00 1,0691+00 1,4974+00 2,1567+00 2,1567+00	1.6278+00 9.935-81 7.5596-81 1.6595-90 1.7549-90 1.0345-90 1.0345-90 1.0345-90 1.0345-90 1.0345-90 1.0345-90 1.275-91 6.7811-81	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	
	9	**	-
1,0691+00 1,0691+00 1,0691+00 1,0691+00 1,0691+00 1,0691+00 2,0691+00 2,0691+00 2,0691+00 2,0691+00		44446 4 5 5 4 5 5 4 4 4 4 5 5 5 5 5 5 5	4,4436-0 -5,9957-01 -6,0619-01 -6,2775-01 -6,8176-01 -1,668-01 -1,668-01
1,8620+00 3,5287+00 2,7082+00 1,7347+00 1,8690+00 1,0118+00 1,0118+00 1,0118+00 2,0568+00 2,7668+00	1.6597400 4.3039-01 6.3734-01 1.8085+00 1.8085+00 1.8926+00 1.0659+00 1.0659+00 1.0659+00 1.0659+00 1.1899+00 1.1899+00	5.0431-01 2.7569-01 2.62031-01 5.62031-01 6.1367-01 3.1903-01 2.6033-01 1.4161-01 1.4403-01 3.20407-01 4.9932-01	4, 2739-01 -5, 9101-01 -5, 1279-01 -5, 1279-01 -1, 1279-01 -1, 7657-01 -9, 9086-02
1,8743+00 3,9685+00 3,6115+00 2,8152+00 1,4717+00 1,1738+00 9,7255-01 1,9660+00 2,6866+00	1.7344+00 5.0154+00 6.0501-01 1.7416+00 1.5398+00 1.5398+00 1.0941+00 7.261-01 5.6124-01 1.1567+00	5.1432-01 3.0766-01 4.7297-02 5.2908-01 6.1991-01 5.2707-01 2.6644-01 1.5419-01 1.9423-01 1.9423-01 1.9423-01	-5.0920-01 -5.0830-01 -6.1685-01 -5.1685-01 -5.1679-01 -1.0747-01
1.8708+00 3.7680+00 3.6715+00 2.9108+00 1.8938+00 1.8938+00 1.2200+00 1.2800+00 1.900+00	1,7658+00 5,8269+00 5,8268+00 1,8577+00 1,8536+00 1,1288+00 1,1288+00 7,7200+01 5,3359+01 1,1273+00	5.229-01 5.3791-01 6.6665-02 7.921-01 4.8646-01 6.2312-01 5.4213-01 2.9055-01 1.6857-01 1.2475-01 1.2475-01 1.2475-01	-3.8969-01 -5.6905-01 -6.1746-01 -5.787-01 -4.9761-01 -3.9461-01 -1.9663-01
1.6334+00 3.4641+00 3.7044+00 2.9907+00 1.5048+00 1.5048+00 1.2742+00 1.2377+00 1.8361+00 2.5608+00	1,7906+00 6,6445-01 5,3601-01 1,4993+00 1,693+00 1,6162+00 1,1677+00 1,1677+00 1,1677+00 1,1677+00 1,1677+00 1,1677+00 1,1677+00 1,1677+00 1,1677+00 1,1677+00	5.2886-01 3.6642-01 6.6101-02 6.5101-02 6.287-01 5.5511-01 2.6958-01 1.668-01 1.668-01 2.8662-01 2.8662-01 2.8662-01	-3,7005-01 -5,5201-01 -6,1853-01 -5,1179-01 -3,4693-01 -2,0919-01
1,7660+00 3,0922+00 3,7364+00 3,0559+00 1,529+00 1,3313+00 9,3277-01 1,760,740 1,760,740 1,760,740 1,760,740 1,760,740 1,760,740 1,760,740 1,760,740 1,760,740 1,760,740	1.00110 1.00110 1.0010 1.0010 1.0010 1.0010 1.0010 1.0010 1.0010 1.0010 1.0010 1.0010 1.0010 1.0010 1.0010 1.0010 1.0010 1.0000	5.3387-01 3.9232-01 1.0666-01 5.749-02 3.9416-01 5.749-01 2.9555-01 2.9555-01 1.1165-01 1.7700-01 2.7464-01 5.3593-01	-3.5043-01 -5.3277-01 -6.0968-01 -5.2019-01 -3.5612-01 -3.5612-01 -3.364-01
1,6896+00 2,7050+00 3,7693+00 3,1135+00 1,5574+00 1,3550+00 9,5374+00 1,6944+00 2,4008+00 3,1203+00	STATION 3 10 1.6105+00 1.6004+00 1.6643+00 1.6643+00 1.6643+00 1.6643+00 1.6643+00 1.6574+00 1.2515+0	222440 22222 22222 22222 22222 22222 22222 2222	57ATION 5
1,6335+00 2,3588+00 3,8226+00 3,1739+00 1,584500 1,4281+00 1,4281+00 1,4281+00 1,624-00 1,624-00 1,624-00 2,3150+00 3,0390+00	2 CHORD 1.84284-00 1.54884-00 1.54884-00 1.8075-01 1.8075-01 1.8075-01 1.8075-01 1.8075-01 1.2075-01 1.0076-00 1.715-00	5.35 6.1417-01 6.1417-01 6.1417-01 6.1417-01 6.1417-01 6.1417-01 6.1616-03 6.161	-3,1349-01 -4,9430-01 -6,0075-01 -5,2695-01 -3,7320-01 -2,3792-01
1.6226+00 2.0966+00 3.2865+00 2.5846+00 1.4560+00 1.4560+00 1.0242+00 1.2201+00 2.2.24+00 2.2.24+00 2.3.24+00	SPAN STATION 1,7878+00 1,5902+00 9,3078-01 3,5962-01 1,652400 1,7155+00 1,3417-00 1,3417-00 1,598-01 7,1226-01 7,1226-01 1,3227+00 1,3227+00 1,5937+00 1,6937+00	5.3725-01 7978-01 7978-01 7978-01 82134-03 8810-01 4212-01 8212-01 7025-01 1525-01 1525-01 1525-01 1525-01	SPAN STATION -2.9568-01 -5.9568-01 -5.9262-01 -5.8624-01 -2.4977-01

Figure 3. Sample Output - Continued.

-4,3979-22 -7,8407-02 -5,2093-02 -7,9482-02 -1,1995-01		6,0799-09 3,2963-00 8,6450-01 1,2014-00 8,8573-00	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		2 + 4541 2 + 4541 5 + 6051 6 + 6051 6 + 6051 6 + 6051 7 + 1051 7 + 10		3,0934-00 3,7926-00 3,9926-00 2,6990-00 2,6990-00 1,7936-00 1,2096-00 1,3995-00 1,5995-00 1,5995-00 1,5995-00
1,5412-02 7,5481-02 1,5450-01 1,572-01			4.1039+00 3.1028+00 3.1028+00 3.1067+00 4.3674+00 6.0051+00 7.6124+00		4.66438+00 7.4964-00 7.4964-00 2.8399-01 2.8399-01 1.3464-00 1.346		3.0873+08 3.4896+00 2.1896+00 2.1714+00 2.1896+00 1.2219+00 1.2219+00 1.2219+00 1.2219+00 1.2219+00 1.0806+00 1.0896+00 2.0001+00
-4.2775-02 -7.3251-02 -7.3096-02 -1.1190-01 -1.7317-01		6,5948+00 3,7725+00 1,2369+00 6,6359-01 2,3173+00	4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		2.664460 7.9879-01 6.6319-01 2.571140 2.9190-00 1.9109-00 1.958-00 1.1958-00 1.7832-00 1.7832-00 2.5707-00		3,0807+00 3,1731+00 2,4669+00 2,4097+00 2,4097+00 2,5038+00 1,2288+00 1,2288+00 1,2128+00 1,2128+00 1,2128+00 1,2128+00 1,2128+00 1,2128+00 1,2128+00 1,2128+00
-6.9488-02 -6.9488-02 -6.9488-02 -6.9188-02 -1.08188-01 -1.08188-01	•	6.8647+00 4.0322+0 1.4270+00 4.3447-01 2.0717+00	4.1884-00 3.2869-00 3.2669-00 3.2660-00 5.1039-00 7.2998-00		2.9018+00 2.9018+00 5.0080-01 2.20808+00 2.20908+00 1.8665+00 1.3587+00 1.2295+00 1.7207+00 2.5032+00		3.0762+00 3.6535+00 2.8789+00 2.8789+00 2.8789+00 1.9409+00 1.2578+00 1.2578+00 1.2578+00 1.3916+00 1.3916+00 1.3916+00
-4,7787-02 -6,5410-02 -6,4660-02 -6,4689-02 -1,0428-01 -1,5205-01	Ì	7,1950+00 4,3163+00 1,6416+00 2,4884-01 1,8758+00	\$ 2046+00 \$ 3059+00 \$ 222+00 \$ 2172+00 \$ 0178+00 \$ 0065+00 \$ 6246+00		4,7465+00 3,1121+00 3,818-01 2,818-01 2,818-01 3,0752+00 1,5342+00 1,2598+00 1,2598+00 1,6717+00 2,4803+00 3,3053+00		3.0709+00 3.9282+00 3.9282+00 3.8229+00 2.8702+00 2.0128+00 1.3118+00 1.3593+00 1.3693+00 1.3693+00 1.3693+00 1.3690+00
-5.3195-02 -6.1684-02 -6.7864-02 -9.9815-02 -1.4447-01		7.5095+00 4.6231+00 1.8896+00 1.6083-01 1.7397+00	4,2220+00 3,4690+00 2,9753+00 2,3282+00 2,9686+00 3,9284+00 5,4474+00		4,6715+00 3,3130+00 9,5490-01 3,5260-01 1,7626+00 2,3782+00 1,6135+00 1,5124+00 1,2660+00 1,2660+00 1,2660+00 1,2660+00 1,2631+00 2,3770+00		3.0594-00 4.1966+00 4.1966+00 4.0935+00 2.9658+00 2.9658+00 1.3918+00 1.3918+00 1.348+00 1.348+00 1.348+00 1.348+00 1.348+00
-5,9692-02 -5,828-02 -7,1642-02 -5,5997-02 -1,3811-01 -2,7816-01		7,8020+00 4,9409+03 2,1675+00 1,7981-01 1,6540+00 3,6394+00	8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9		4.5202+00 1.079+00 1.079+00 1.079+00 1.0195-01 1.561+00 2.462+00 1.7016+00 1.2959+00 1.0113+00 1.5921+00 2.3077+00 2.3077+00		3,039940 4,391140 4,3911400 4,555640 2,9532400 2,469400 1,1394400 1,1394400 1,3061400 1,3061400
-6.6475-02 -5.5074-02 -5.2878-02 -5.2878-02 -9.0686-02 -1.3255-01	STATION 1	8-0435-00 5-2536-00 2-4616-00 1-5911-00 3-4656-00		ATION 2	#.3486+00 3.7370+00 1.5562+00 3.5159-01 1.3996+01 3.2912+00 1.3912+00 1.3912+00 1.3410+00 1.0193+00 1.5475+00 3.0193+00 3.0193+00	STATION 3	3.0123+00 4.4497+00 4.7507+00 4.7507+00 2.8294+00 2.8294+00 1.5906+00 1.1487+00 1.1231+00 1.231+00 1.2625+00
-7.2979-02 -7.1847-02 -7.51757-02 -5.1164-02 -8.6537-02 -1.2756-01	CHORD	6.2104+60 5.5461+00 2.7540+00 4.6529-01 1.5141+00 3.3096+00	4.298e+00 3.825.4+00 2.3273+00 3.0393+00 3.676.40 4.9673+00 6.4583+00	CHORD ST	4,1610+00 3,9766+00 1,5109+00 1,5109+00 1,2616+00 3,2866+00 2,8643+00 1,8454+00 1,0454+00 1,0454+00 2,1406+00 2,1406+00 3,7494+00	CHORD	2,9014+00 3,0700+00 4,3479+00 4,6330+00 2,6007+00 2,502+00 1,6779+00 1,15779+00 1,1527+00 1,1527+00 1,2090+00 1,5568+00
-7.9086-02 -7.8586-02 -7.8794-02 -5.095-02 -6.2906-02 -1.2307-01	SPAN STATION 3	8.2907+00 5.8197+00 3.0303+00 6.6600-01 1.3696-00 3.1011+00	4.3106+00 3.9345+00 2.965+00 3.2976+00 3.0791+00 3.5579+00 6.2956+00 7.9370+00	SPAN STATION 3	4.0340+00 1.7229+00 1.7229+00 1.7229+00 5.5520+00 3.2119+00 2.220+00 1.3073+00 1.3073+00 1.4247+00 2.4236+00 2.8236+00 2.8236+00 2.8236+00 2.8236+00 2.8236+00	SPAN STATION 3	2,9225+00 4,1065+00 3,0363+00 4,2441+00 2,3464+00 2,3464+00 1,407+00 1,1873+00 1,1873+00 1,18556+00 1,1525+00 1,5838+00

Figure 3. Sample Output - Continued.

											ī								!					- (- 6		1			1				- 1		
	2.6134+00		2934-01 7980-01	0781-01	9049-05	1961-02	7016-02	3446-03	5843-08	1995-01		-7.2044-01	. 5036-01	10-57-01	10-9966	1005-01	2346-01	2.8625-01	-2,6949-01	0-020-	10-10-1	.6592-01	.5008-01	1		6.1488+00	7278+00	4004-00	AESA+00	0003+00	7150+00	8197+00	1082400	4173+00	2062+00	8776+00		,
	2.7578+00		-1.7199-02 -3.8050-01 -7.7911-01	5.2221-01	17-02	20-05	76-02	2.9063-02	2 2 706-02	2.5633-01		-7.0132-01	-0.4629-01	-8.0331-01	-7.4199-01	10-35-16-17	-3.2800-01	-2.8397-01	-2,6761-01	-2.9591-01	2.5024-01	-3.6264-01	4.3716-01			6.4913+60	8	4907-00	3510+00	1020+00	8051+00	8783400	1052+00	1479-00	9407+00	5345+00		
	2.6918+00		1.1192-02-5.3302-01			-5.6321-02	-4.9664-02			2.6171-01					-7.4465-01		-3.3387-01				10-01-01		-4.2568-01			6.8407+00	4.0894+00	1.6581+00	1.3016+00			2.9342+00						
	2.6201+00		3.8924-02-2.8754-01	-6.4752-01	-8.9869-02					2.5944-01		-6.6496-01	-6.3131-01	-6.1890-01	-7.4572-01	10-60-6	-3.4133-01	-2.9315-01	-2,6629-01	-2.8886-01	-2.0042-01	-3.7364-01	-4.1610-01			7.1808+00	4,2940+00	1.9011+00	1.2948+00	4.0499+00	3.9248+00	3.0077+00	3.1455+00	3.6753+00	5,5272+00	9,3360+00		
	2.5466+00		6.5381-02 -2.4470-01 -7.1177-01				-6.3758-02		3497-02	2,5137-01		-6.4716-01	-6.2078-01	-8,2654-01	-7.4735-01	- 4- 6464-01	-3.5032-01				10-0616.7		-4.0785-01		٠	7.4964+00	5154+00	2 1996+00	3148+00	9834+00	9596+00	2.0891+00	1786+00	5030+00	2044400	2262+00		
	2.4733+00		9.0002-02 -2.0501-01 -6.7183-01				-7.4533-02		1.8635-02	2.3789-01		-6,2881-01	-8.0824-01	-8.3408-01	-7.5103-01 -4.557-01	4.8257-01	-3.6045-01		-2,6819-01				-4.0121-01			7.7850+00	4.7496+00	2.5221+00	2.0407+00	3.8631+00	3.9856+00	3.1786+00	3-1965+00	3.3753+00	5.2928+00	9.1235+00		
	2,9285+00		70				-8.6796-02		2,3638-02	2,1995-01		-6,0934-01	-7,9366-01	-8.4107-01	-7.5729-01 -4.5448-01	-5.0052-01	-3.7109-01	-3,0820-01	-2,6995-01	-2.8022-01	-3.0260-01	-3.5694-01		-5,2181-01		6.0504+00	4.9939+00	2,6354+00	1.5793400	3,7449+30	4.0089+10	3,2772,00	3,2030+00	3,2831+00	5.1936+00	9.0252+00	9.0547+00	
	2,9079+00	AT10N 4	1.3310-01 -1.3523-01 -5.7660-01	-7.3607-01	-1,4466-01							-5.8849-01	-7.7714-01	-6.4681-01	-7.6575-01 -6.8355-01	-5 1706-01	-3.8162-01	-3,1246-01	-2.7204-01	-2.7748-01	-2.9472-01	-3,5233-01	-3.9270-01	-2,0087-01	STATION 1	8.3034+00	5,2506+00	3,1150+00	1.3655+00	3,5681+00	4.0332+00	3.3848+00	3,1907+00	3,2157+00	5.0661+00	6.9160+00	9.2760+00	STATION 2
0017666	2.8856+00	CINORD ST	5							1,7685-01	CHORD S	=		-6.5057-01		-5.3112-01							-3.9024-01		4 CHORD S'	8,5549+00	5,5252+00	3.3514+00	1.6958+00	3,3576+00	4.0586+00	3.4981+00	3,1612+00	3,1652+00	4.8963+00	8.7785+00	9.4484+00	CHORD
0.00	2.8558+00	SHAN STATION 3	1.7042-01-7.4661-02							1.5548-01		-5,4397-01			7.6536-01								-3,8820-01		SPAN STATION	8.8080+00	5,8239+00	3.5502+00	1.5633+00	3,1246+00	4.0820+00	3,5111+00	3,1197+00	3,1289+00	00+64/004	8.6021+00	9.5522+00	SPAN STATION 4

Figure 3. Sample Output - Continued.

4,0649+00 2,9050+00 1,7842+00	1.6242+00	2.0565+00	1.8761+00	1.5727+00	1.40400	2.2792+00	2,8941+00	3,6555+00	3.9628+00			1.3034+00	1.1375+00	10-0017-7	4249-00	7.9656-01	7.0311-01	-	1220	NAME OF	7264-00	2,1075+00	2.2172+00				4.1866-01	10-046	4.2310-01	4.1561-01	4,2134-01	4.2825-01	10-1402.	4.2503-01	4.3191-01	4.3267-01	4.4148-01	4.4110-01			-2,9057-01 -2,1857-01 -2,1919-01 -1,0476-01	
4.2016+00 2.9754+00	1.5891+00	1.9210+00	1.9311+00	1.3916+00	1. 1004400	2,1707+00	2.7946+00	3.5634+00	3.9604+00			0			1,3222+00			10-91					2,2783+60				4.2066-01	1759-01	4.2334-01	4.1348-01	4.2167-01	# .2839-01	4 2440-01	2509-01	4.3253-01	4.3327-01	4.4205-01	4.4190-01			-2.9763-01 -2.2041-01 -2.4007-01 -9.9063-02	
4,3096+00 3,0496+00 1,9312+00	1.5633+00	1.6151+00	1,9757+00	1.4169+00	1-6031+00	2.0629+00	2.7132+00	3,4609+00	2.9606+00			0			1.0743+00			6.2236-01	10-0-16-7	10-43/4-01	1.5615+00	1.9735+00	2.2925+00				4 2322-01	4.1657-01	4.2311-01	4.1172-01	4.2164-01	4.2744-01	4.2547-01	4.2685-01	4.3306-01	4.3414-01	4.4218-01	4,4203-01			-2,9676-01 -2,2277-01 -2,5444-01 -9,6658-02	
4.3785+00 3.1339+00 2.0624+00	1.5528+00	1.7445+00	2,0137+00	1.4485+00	1.6115+00	1.9629+00	2.6549+00	3,4132+00	3. 9020+00			0			7.3542-01			6.2277-01	10-2666	1,1414+00	1.5144+00	1.9025+00	2.2645+00				4.2614-01	4.1548-01	4.2271-01	4.1084-01	4.2136-01	4.2563-01	A . 2555-01	4.2711-01	4.3303-01	4.3487-01	4.4171-01	4.4159-01			-2.8489-01 -2.6070-01 -9.7962-02	
4.4020+00 3.2310+00 2.2110+00	1,5586+00	2.6799+00	2.0517+00	1.4880+00	1.6206+00	1.8748+00	2.6173+00	3,3587+00	3.4040400			1.5540+00	1.7262+00	-3.1169-01	3.7906-01	5,1329-01		7200-01	10-992/ 0	1,1125+00	1.5049+00	1.8545+00	2,2147+00			.0	4.14.14.01	4.1807-01	4.2231-01	4.1117-01	4.2102-91	4.2344-01	4.2462-01	4.2653-01	4.3215-01	4,3511-01	4.4057-01	4.4086-01			-2,713-01 -2,2713-01 -2,5900-01 -1,0329-01	
8,3819+00 3,3422+00 2,3646+00	1.5769+00	2.6528+00	2.0967+00	1.5371+00	1.6269+00	1.7999+00	2.5912+00	3.3098+00	2.9540100			1,7557+00	10-005/100	-2.6271-01	7.3299-02	5.5656-01		7 2752-01				8372+00				.0.00	4-1636-01	4.1219-01	4.2195-01	4.1271-01	4-2074-01	4.2147=01	4.2324-01	4.2526-01	4.3046-01	4.3472-01	4.3888-01	4.4013-01			-2.5464-01 -2.3089-01 -2.5121-01 -1.1300-01	
4.3273+00 3.4679+00 2.5101+00	1.6018+00	2.5877+00	2,1538+00	1.5966+00	1.6262+00	1,7374+00	2,5639+00	3,2560+00	4.0436+00			1.9079+00	1.9391+00	-2.4542-01	-1,4033-01	7.0696-01	5,8371-01	5.5997-01	0.0110-01	1.0627+00	1.5485+00	1,8427+00	2,1418+00	1,9470+00		10-7101 4	4 1758-01	4.0988-01	4,2156-01	4,1512-01	4 2047-01	4.2018-01	4.2196-01	4.2376-01	4,2833-01	4,3383-01	4,3690-01	4,3968-01	10-2045		-2,3779-01 -2,4045-01 -1,2740-01	
4,2522+00 3,6070+00 2,6379+00	1.6291+00	2.4863+00	2,2251+00	1.6651+00	1.6242+00	1,6867+00	2,5234+00	3,1880+00	4.0050+00	STATION 3		+##86	2010	03-01	42-01	96-01	33-01	75-01		68+00	00+11	16+00	2,1378+00	29+00	ATION 4	10-10-1	4 1794-01	4.0742-01	4.2102-01	4,1765-01	4.2000-01	19/2-01	4 2127-01	4.2261-01	4.2632-91	4.3276-01	4.3498-01	4.3964-01	10-1200	ATION 5	-2,2478-01 -2,4854-01 -2,3002-01 -1,4648-01	
4,1721+00 3,7571+00 2,7440+00	1,6589+00	2.3552+00	2.3085+00	1.7384+00	1.6151+00	1,6475+00	2,4622+00	3,1018+00	3.9617+00	CHORD		1,9927+00			-2.9515-01								2,1431+00		CHORD ST	1344-01	4-1786-01	4.0530-01	4.2030-01	4.2033-01	4.1910-01	4.2004-01	4-2144-01	4.2222-01	4.2496-01	4.3193-01	4.3349-01	4.4003-01	TO-1610*	CHORD ST	-2,1652-01 -2,6264-01 -2,2243-01 -1,6947-01	
4.1000+0U 3.9127+00 2.8308+00	1.6962+00	2.2067+00	2.3986+00	1.8107+00	1-604	1.6199+00	2.3792+00	3-0000-00	3.9690+00	SPAN STATION 4		1.9663+00		-2.1798-01								1.7995+00	2.1381+00	2.1247+00	SPAN STATION 4	4.1305-01	4.1803-01	4.0405-01	4.1941-01	4.2213-01	4.1760-01	10-1702-4	4.2229-01	4.2271-01	4.2455-01	4.3163-01	4.3269-01	4.4072-01	Torroccit	SPAN STATION 4	-2.1187-01 -2.7778-01 -2.1876-01 -1.9461-01	

Figure 3. Sample Output - Continued.

-1,4472-01 -1,0747-01 -9,9401-02 -1,5580-01 -1,6193-01 -1,655-01 -1,562-01 -1,562-01	3,7365+00 1,5712+00 1,0525+00 2,6081+00 2,0462+00 2,0462+00 2,0919+00 2,7210+00 3,7230+00 6,9767+00 6,9767+00	3,0741+00 1,193+00 1,693+00 -1,0313+00 -1,0513+00 2,131-01 8,5421-01 8,5421-01 8,5421-01 1,7661+00 2,0423+00 2,0423+00	-2, 3612+60 -1, 0117+80 -2, 0401+80 -1, 9971+00 -1, 1694-00 -5, 3259-01 -2, 6669-01 6, 2240-62
1,434-01 -1,1384-01 -9,5471-02 -1,5804-01 -1,6964-01 -1,6964-01 -1,13478-01 -1,3478-01 -1,3478-01	4,1856+00 1,6693+00 1,5776-01 1,1776-01 2,6394+00 2,0304+00 2,0713+00 2,3401+00 2,3401+00 3,5864+00 5,0204+00 6,6323+00	2,8252+00 2,8317-01 2,3317-01 2,3477-01 2,3477-01 2,3477-01 1,2813-01 1,2813-01 1,2813-00 1,2813-00 1,2813-00 2,0124+00 2,0124+00 2,0124+00	2,0884-00 1,08312+00 2,0205+00 2,03115+00 1,2317+00 5,935-01 3,526-01
-1.4529-01 -1.2527-01 -1.2527-01 -1.25411-01 -1.2539-01 -1.2393-01 -1.3973-01	4,6661+00 1,7523+00 2,0340-01 2,0340-01 2,0340-01 2,0340-01 2,03400 2,047740 2,2525+00 2,2535+00 4,0617+00 6,4185+00 6,4185+00	2.4073-00 3.5112-01 -6.3563-01 -6.3653-01 2.4972-01 8.6810-01 7.0469-01 6.5731-01 1.1896-00 2.0295-00 2.0295-00	-1,6424+00 -1,0999-00 -1,6967+00 -2,0460+00 -2,1918+00 -1,3304+00 -5,5621-01 -1,1508-02
1,4660-01 -1,3467-01 -8,6970-02 -1,1962-01 -1,2164-01 -1,5976-01 -1,3996-01 -1,3996-01	5,1486+00 1,8373+00 2,5173+01 7,7616-01 2,6792+00 2,1293+00 2,1293+00 3,1025+00 6,3151+00 9,3417+00	1,9310+00 1,2172+00 2,3129-01 2,3129-01 2,2610-01 4,2759-01 6,5359-01 1,0899+00 1,6496+00 2,0533+00 2,0533+00	-1,5040+00 -1,4305+00 -1,6124+00 -2,0927+00 -2,0954+00 -1,4176+00 -6,9908-01 -3,9702-01
1,4687-01 -1,4283-01 -6,7464-02 -1,1549-01 -1,6524-01 -1,339-01 -1,4016-01 -1,4016-01	5.6457400 1.9456400 5.29627-01 6.2962-01 2.473400 2.1706400 2.1516400 2.9565400 6.2737400 9.3431400	1,5173+00 1,3686-00 5,0540-01 -1,1161-01 1,4057-01 4,5733-01 6,2182-01 9,9678-01 1,6210-00 2,0591+00 2,0591+00	-1,0934+00 -1,9116+00 -1,5904+00 -2,1689+00 -1,9156+00 -7,3965-01 -1,2467-01
-1.4481-01 -1.4860-01 -8.7408-02 -1.1225-01 -1.5101-01 -1.5101-01 -1.3770-01 -1.4189-01 -1.4089-01	6.1435400 2.0972400 2.2045401 2.2045401 2.5045400 2.2259400 2.8358400 6.2352400	1.2601+00 5.9947+01 5.9947+01 -6.4730+02 -1.1069+02 4.3945+01 6.0631-01 6.0631-01 1.5831+00 2.351+00	-9,8502-01 -2,4430+00 -1,5966+00 -2,2633+00 -1,6356+00 -7,6066-01 -7,6066-01 -7,285-01
-1,3978-01 -1,5135-01 -8,6735-02 -1,0968-01 -1,2263-01 -1,4197-01 -1,3286-01 -1,4251-01 -1,4251-01	6.62840 2.3068400 -1.3068400 3.3068400 3.8407-01 2.1550400 2.5558400 2.7558400 2.7352400 4.5346400 6.1497400 6.1497400	1.1998+00 2.0930+00 2.0930+00 1.54672-02 2.1114-01 3.0890-01 5.0890-01 8.6699-01 1.5407+00 1.9712+00 2.3352+00	-9,2409-01 -2,8991+00 -1,5866+00 -2,3464+00 -1,8168+00 -1,8168-00 -8,318-01 -4,2359-01
-1,3203-01 -1,5123-01 -9,1342-02 -1,0793-01 -1,2695-01 -1,4657-01 -1,4657-01 -1,4657-01 -1,4667-01 -1,464-01 -1,464-01	7.0825400 1.1225400 1.1225400 1.0857-01 2.6931-01 1.687-01 2.653400 2.553400 2.553400 4.3908400 8.4694400 8.4694400	2.532400 8.5375-01 -4.5622-01 -4.2662-01 5.0957-01 5.0957-01 8.881-01 1.49881-01 1.49881-01 2.0739+00 2.0739+00	-0.5335-01 -3.1683+00 -1.5114+00 -2.3810+00 -1.6494+00 -2.0477+00 -9.0061-01 -2.257-01
-1,2260-01 -1,4918-01 -9,5237-02 -1,0577-01 -1,2906-01 -1,1881-01 -1,4883-01 -1,2591-01 -1,2591-01	7.4669400 2.9159400 1.296u+00 -4.0720-02 1.5364-01 1.7846+00 2.46474+00 2.46474+00 2.46474+00 2.46474+00 2.46474+00 2.46474+00 2.46474+00 2.46474+00 2.46474+00 2.46474+00 2.46474+00 2.4644+00 2.4644+00 2.4644+00 3.5654+00 3.5654+00 5.5644+00	2,88546 2,8897400 -3,7855-01 -1,5167400 -6,2255-01 4,9977-01 8,9511-01 8,784-00 1,4578-00 2,0170-00 2,0170-00	-7,3682-01 -3,1882+00 -1,3623+00 -2,3396+00 -2,2191+00 -9,8502-01 -4,4210-01
-1.1300-01 -1.4657-01 -1.0056-01 -1.0295-01 -1.4149-01 -1.4569-01 -1.5293-01 -1.5293-01 -1.752-01	7.6284+00 1.4474+00 1.4474+00 3.1129-02 3.6855-02 1.5713+00 2.6853+00 2.6853+00 2.6853+00 2.6853+00 2.6853+00 2.6853+00 2.6853+00 2.6853+00 2.6853+00 2.6853+00 2.6853+00 2.6853+00 2.6853+00 2.6853+00 2.6853+00 2.6853+00 3.667+00 5.667+00 5.667+00 5.667+00	1,7821+00 1,102+00 1,009+00 6,996+02 -1,3151+00 -77536-01 2,1241-01 4,7283-01 8,6699-01 1,4128+00 2,0814+00 2,0648+00 SPAN STATION	-5.7085-01 -2.9634+00 -1.1721+00 -2.179+00 -1.9594+00 -2.335+00 -1.0776+03 -4.7901-01

Figure 3. Sample Output - Continued.

						•	
 | | | | |
 | | | | á |
 | | | | - |
 | | | | |
 | | | | 1 |
 | , | |
|-----------|---|---|---|--|--|--|--
--	--	--	---
--	--	--	--
--	--	--	---
--	--	--	--
--	--	--	--
--	---	--	--
3.1676-01	2.9166-01	5.0771-02	
 | 00+CC20*I- | 11.1009+00 | | -6.9307-01 | -3.1672-01
 | -3.6605-01 | -2.5851-01 | 1-382-61 | -7.2719-01 | -1,1032+00
 | | | | | -6.2882-01
 | 1000 | 10-1/9/ | 100/001 | | 0414
 | 3.6939-01 | -3.6480-01 | 3.9012-01 | 5.2784-01 | 6.2110-01
 | -7,2554-01 | |
| 2 | 7680-0 | 3142-0 | | | | | 2.2662+00 | 5220+00
 | 1 | 8840-0 | 9631-0 | 0-5450 | 2313-0
 | 5732-0 | 0-9969 | 7091-0 | 0263-0 | 0217+00
 | | | | | -6.4550-01
 | -5,2101-01 | -3.5165-01 | 10-70-1 | | 0000
 | -3.6932-01 | -3.6865-01 | -3.8563-01 | -5.1577-01 | -6.1767-01
 | -7,1134-01 | |
| 2000 | 9901-0 | 0704-0 | | | | -1.9476+00 | -2.2819+00 | -1.6891+00
 | 10-9224·6 | 00-11-0-1 | 4771-61 | 1000-01 | -3,3070-01
 | -3.5996-01 | -2.8307-01 | 4.4613-01 | -6.7681-01 | -9.4734-01
 | | | | -7.5546-01 | -6.6510-01
 | -5.6022-01 | -3.2508-01 | 10-26-11 | | -4.0220-01
 | -3.6817-01 | -3.7100-01 | -3.8147-01 | -5.024A-01 | -6.1363-01
 | -6.9655-01 | |
| 2.5337-01 | 3.5044-01 | 1.6660-01 | | | | -1.9025+00 | -2.2578+00 | -1.844400
 | 10-01-07-0 | 00+19/7-1- | -4-6110-01 | -5.1842-01 | -3.4074-01
 | -3.5499-01 | -2.9445-01 | -4.2014-01 | -6.5092-01 | -8.8655-01
 | | | | -7.6410-01 | -6.0449-01
 | -5.8926-01 | -3.0961-01 | 10-6061 | 1010000 | 10-11-01
 | -3.6650-01 | -7.7140-01 | -3.7665-01 | -4.8730-01 | -6.0802-01
 | -6.8186-01 | |
| 2.1404-01 | 4,0996-01 | 2.4699-01 | | , | | -1.8350+00 | -2,2142+00 | 00+2676.1-
 | 10-0002-6- | -9.7057-01 | -6-9462-01 | -5.3099-01 | -3.5531-01
 | -3-4399-01 | -3.0170-01 | -3,8655-01 | -6.2539-01 | -6.4230-01
 | | . ** | | -7.7129-01 | -7.0092-01
 | -6,0691-01 | -3.0028-01 | 4 4171-01 | - 053k-01 | -4 .062A-01
 | -3,6543-01 | -3.7016-01 | -3.7101-01 | -4.7022-01 | -5.9990-01
 | -6,6794-01 | |
| 1.6658-0 | 4.5296-0 | 3.2796-01 | | | | -1.7511+00 | -2.1573+00 | 00-10/0-0-
 | 10-100-1- | -1.0073+00 | -7.3487-01 | -5.4824-01 | -3.7553-01
 | -3.3052-01 | -3.0549-01 | -3.4940-01 | -6.0024-01 | -6.1327-01
 | | | | -7.76-1-01 | -/-1293-01
 | 10-96-01 | 10-10-10-1 | 4.4278-01 | -3.965A-01 | -4.0921-01
 | -3.6614-01 | -3.6820-01 | -3.6525-01 | -4.5204-01 | -5.8950-01
 | -6.5537-01 | |
| 1,2107-01 | 4.6252-01 | 3,8498-01 | -3,8014-01 | | | -1.6608+00 | -2.0976+00 | -0 6749-01
 | 2716100 | -1.0428+00 | -7.7603-01 | -5.6811-01 | -4.0091-01
 | -3,1858-01 | -3,0849-01 | -3,1295-01 | -5,7556-01 | -7.9480-01
 | -1,3777+00 | | | 10-/69/-/- | 10-4502-1-
 | -0.1464-01 | 10-00-01 | -4-3987-01 | -4.0134-01 | -4.1283-01
 | -3,6934-01 | -3,6664-01 | -3,6055-01 | -4.3419-01 | -5,7740-01
 | -6.4459-01 | -7,6673-01 |
| 8.8735-02 | 4.3676-01 | 4.0173-01 | -2.0202-01 | TATION 4 | | | | 1 0202400
 | 2215400 | 00+8+00 | 1219-01 | 8699-01 | -4.2888-01
 | -3,1111-01 | -3,1373-01 | | -5,5183-01 | -7.8097-01
 | -1.3207+00 | TATION 5 | | 7 2610 | 10-0162
 | 10-0971 | -4 2830-01 | -4 3500-01 | -4.0863-01 | -4.1629-01
 | -3,7490-01 | -3,6620-01 | -3,5806-01 | -4.1829-01 | -5,6455-01
 | | -7.5925-01 |
| 7.6358-02 | 3,8914-01 | 3.7869-01 | -6.7409-02 | | | -1.4987+00 | -2 2277400 | -1.1020+00
 | -1.1562400 | -1.1042+00 | -6.3980-01 | -6.0165-01 | -4.5563-01
 | -3.0907-01 | -3,2289-01 | -2.6246-01 | -5.2972-01 | -7.6664-01
 | -1,2569+00 | | | 10-0501.7- | 10-1007-1-
 | 10-1202101 | -4-1736-01 | -4.2867-01 | -4.1702-01 | -4.1836-01
 | -3,6193-01 | -3,6695-01 | -3,5830-01 | -4.0554-01 | -5,5180-01
 | -6.2932-01 | -7.4984-01 |
| 8.2836-02 | 3.4188-01 | 3-3317-01 | 1,2837-02 | SPAN STATION 5 | | -1.4346+00 | 00+6164-1- | -1-2161+00
 | -1-0866+00 | -1.1338+00 | -8.5899-01 | -6.1100-01 | -4.7761-01
 | -3.1155-01 | -3,3529-01 | -2.5480-01 | -5.0 9 51-01 | -7.4890-01
 | -1:163/+00 | SPAN STATION | | TO=202/0/ | TO-OLACO V
 | 10-06/1-0- | -3-9959-01 | -4-2205-01 | -4.2511-01 | -4.1794-01
 | -3.8909-01 | -3.6829-01 | -3.6095-01 | -3.9634-01 | -5,3962-61
 | -6.2460-01 | -7.3853-01 |
| | 7.6356-02 8.8755-02 1.2107-01 1.6658-01 2.1404-01 2.5337-01 2.604-01 2.5337-01 2.504-01 | 7.6356-02 6.8735-02 1.2107-01 1.6658-01 2.1404-01 2.5337-01 2.9040-01 2.9040-01 3.2165-01 3.7791-01 4.1736-01 4.6252-01 4.5296-01 4.0996-01 3.5544-01 2.9901-01 2.7400-01 | 7.6356-02 8.8735-02 1.2107-01 1.6658-01 2.1404-01 2.5337-01 2.9040-01 2.9060-01 2.7791-01 4.1756-01 4.8830-01 4.5829-01 4.0996-01 3.5044-01 2.9901-01 2.7960-01 3.5044-01 2.9901-01 2.7960-01 3.5044-01 2.9901-01 7.3142-01 3.7660-01 1.6660-01 1.0704-01 7.3142-02 | 7.6356-02 8.8735-02 1.2107-01 1.6659-01 2.1404-01 2.5337-01 2.9040-01 3.7791-01 4.1736-01 4.4830-01 4.5829-01 4.5119-01 4.0155-01 3.5544-01 3.5544-01 3.5544-01 2.9901-01 2.9901-01 2.9901-01 2.9901-01 2.9901-01 2.9901-01 2.9901-01 2.9901-01 2.9901-01 2.9001-01 2.9901-01 2.9901-01 2.9001 | 7.6558-02 8.8755-02 1.2107-01 1.6658-01 2.1404-01 2.5337-01 2.996-01 2.996-01 3.7791-01 4.1736-01 3.5546-01 3.5546-01 3.5546-01 3.5546-01 3.5546-01 3.5546-01 3.5546-01 3.5546-01 3.5546-01 3.7590-0 | 7.6558-02 8.8755-02 1.2107-01 1.6658-01 2.1404-01 2.5337-01 2.994-01 2.9948-01 3.7791-01 4.1736-01 3.5545-01 3.5545-01 3.5545-01 3.5545-01 3.5545-01 3.5545-01 3.5545-01 3.5545-01 3.5545-01 3.5545-01 3.5545-01 3.5545-01 3.5545-01 3.5545-01 3.5545-01 3.5545-01 3.5545-01 3.5545-01 3.5650-01 3.6550-01 3.5650- | 7,6356-02 8,8735-02 1,2107-01 1,6659-01 2,1404-01 2,5337-01 2,600-01 2,500-01 3,504-01 3,504-01 3,504-01 3,504-01 3,504-01 3,504-01 3,504-01 2,760-01 3,760- | 7,6356-02 6.8735-02 1.2107-01 1.6659-01 2.1004-01 2.5337-01 2.800-01 2.800-01 3.7791-01 4.1730-01 4.4630-01 4.6630-01 4.0185-01 3.5044-01 2.9001-01 2.7600-01 3.7791-01 4.3675-01 4.6552-01 4.5252-01 4.0185-01 3.5044-01 2.9901-01 2.7600-01 3.7869-01 3.5044-01 2.9901-01 2.7600-01 3.7869-01 3.7869-01 3.5044-01 2.9901-01 2.78000-01 2.78000-01
2.78000-01 2.78000- | 7.6356-02 6.8735-02 1.2107-01 1.6659-01 2.1404-01 2.5337-01 2.690-01 2.5337-01 2.690-01 2.5337-01 2.690-01 2.5337-01 2.690-01 2.690-01 2.690-01 3.590-01 3.590-01 3.590-01 3.590-01 3.590-01 2.9 | 7,6356-02 6,8735-02 1,2107-01 1,6659-01 2,1404-01 2,5337-01 2,000- | 7,6356-02 6,8735-02 1,2107-01 1,6659-01 4,119-01 2,5337-01 2,5901-01 2,901-01 2,901-01 3,7791-01 4,1730-01 4,4630-01 4,6430-01 4,0496-01 3,5044-01 2,901-01 | 7.6356-02 6.8735-02 1.2107-01 1.6659-01 4.019-01 2.5337-01 2.900-01 2.5337-01 2.900-01 2.5337-01 2.900-01 2.5337-01 2.900-01 2.90 | 7.6356-02 6.8755-02 1.2107-01 1.6659-01 4.190-01 2.5337-01 2.900-01 2.5337-01 2.900-01 2.5337-01 2.900-01 2.5337-01 2.900-01
2.900-01 2.90 | 7.6356-02 6.8735-02 1.2107-01 1.6659-01 4.119-01 2.5337-01 2.900-01 2.5337-01 2.900- | 7.6356-02 6.8735-02 1.2107-01 1.6659-01 4.119-01 2.337-01 2.357-01 | 7.6356-02 6.8735-02 1.2107-01 4.629-01 4.019-01 2.5337-01 2.590-01 3.590-01 2.590-01 3.590-01 2.590-01 3.590-01 2.590-01 3.590-01 2.290-01 2.590-01 | 7,6356-02 6,8735-02 1,2107-01 4,680-01 4,619-01 2,5337-01 2,590-01 3,504-01 2,590-01 3,504-01 2,590-01 3,504-01 2,590-01 | 7.6556-02 6.8735-02 1.2107-01 4.8830-01 4.8199-01 2.3337-01 2.854-01 2.8337-01 2.854-01
2.854-01 2.854 | 7.6558-02 6.8735-02 1,2107-01 4,6820-01 2,104-01 2,5337-01 2,590-01 3,550-01 3,500-0 | 7.5556-02 6.8735-02 1.2107-01 1.6559-01 4.4119-01 2.5337-01 2.599-01 3.5155-01 3.7791-01 4.759-01 4.6252-01 4.6252-01 4.6252-01 4.6252-01 1.65600-01 1.65600-01 1.65600-01 1.65600-01 1.65600-01 1.65600-01 1.65600-01 1.65600-01 1.65600-01 1.65600-01 1.65600-01 1.65600-01 1.65600-01 1.66600-01 1 | 7.6356-02 6.875-02 1.2107-01 4.625-01 4.629-01 2.469-01 2.5337-01 2.660-01 1.070-01 2.990-01 2.990-01 3.5504-01 3.5504-01 3.5504-01 3.5504-01 2.990-01 3.5504-01 2.990-01 3.5504-01 3.5504-01 3.5504-01 3.5504-01 3.5504-01 3.5504-01 3.5504-01 3.5504-01 3.5004-01 3.5504-01 3.5004 | 7,6556-02 6.8735-02 1,2107-01 1,6656-01 2,1406-01 2,5537-01 2,5046-01 3,7794-01 4,1136-01 4,1136-01 4,1136-01 1,2554-01 3,7594-01 1,2756-01 4,1136-01 4,1136-01 1,2564-01 1,2756-01 2,1256-01 1,2756 | 7,6356-02 6,6735-02 1,2107-01 1,6656-01 2,5406-01 2,5337-01 2,560-01 3,7751-01 4,136-01 4,6406-01 1,6660-01 1,070-01 2,760-01 3,7751-01 4,555-01 1,0556-01 1,070-01 1,070-01 2,760-01 3,6496-01 1,070-01 1,070-01 2,760-01 1,070-01 1,070-01 2,760-01 1,070-01
1,070-01 | 7.6356-02 6.6735-02 1.2107-01 1.6659-01 2.1404-01 2.3337-01 2.590-01 3.590-01 3.7711-01 4.1736-01 4.6550-01 4.6550-01 4.6550-01 1.0074-01 2.7650-01 3.7711-01 4.1736-01 3.6750-01 4.6550-01 1.0074-01 2.7650-01 1.0074-01 2.7650-01 1.0074-01 2.7650-01 2.7650-01 2.7650-01 1.0074-01 2.7650-01 2.7650-01 1.0074-01 2.7650-01 2.7650-01 1.0074-01 2.7650-01 2.7650-01 1.0074-01 2.7650-0 | 7,6559-02 6,8735-02 1,2107-01 1,6659-01 2,1949-01 2,5337-01 2,599-01 3,599-01 3,599-01 3,599-01 3,599-01 3,599-01 3,599-01 1,079-01 4,1739-01 4,1739-01 4,1739-01 4,1739-01 2,999-01 1,6669-01 1,079-01 2,999-01 2,599-01 2 | 7,5956-02 6,8735-02 1,2107-01 1,6556-01 2,1646-01 2,5337-01 2,566-01 1,5791-01 4,779-01 4,779-01 4,779-01 4,779-01 4,7795-01 4,579-01 4,579-01 4,579-01 4,579-01 1,5879-01 1,5879-01 1,5879-01 1,5879-01 1,5879-01 1,5879-01 1,5879-01 1,5879-01 1,5879-01 1,5879-01 1,5879-01 1,5879-01 1,5879-01 1,5879-01 1,5879-01 -2,1879- | 7,5956-02 6,8735-02 1,2107-01 1,6556-01 2,1404-01 2,5337-01 2,544-01 2,544-01 4,775-01 4,750-01 4,750- | 7,6356-02 6,675-02 1,2107-01 1,6650-01 4,825-01 3,504-01 2,5337-01 2,5901-01 2,746-01 3,504-01 3,504-01 2,746-01 3,504-01 3,504-01 3,504-01 3,504-01 3,504-01 3,504-01 3,504-01 3,504-01 3,504-01 3,504-01 3,504-01 3,504-01 3,504-01 3,504-01 3,504-01 3,504-01
3,504-01 3,504-0 | 7.6556-02 6.8755-02 1.2107-01 1.6656-01 1.6656-01 1.6660-01 1.676-01 2.765- | 7,6356-02 6,873-02 1,2107-01 1,6650-01 2,6650-01 3,5040-01 2,5040-01 3,5040- | 7.6356-02 6.873-02 1.2107-01 1.6659-01 2.1004-01 2.5337-01 2.596-01 3.596-0 | 7.6356-02 6.775-02 1.2107-01 1.6650-01 2.1804-01 2.5337-01 2.884-01 3.884-0 | 7,6356-02
6.775-02 1.1070-01 8.252-01 8.253-01 1.0060-01 1.078-01 2.200-01 3.500-01 | 7.6356-02 6.775-02 1.1070-01 8.259-01 8.259-01 1.6660-01 1.078-01 2.289-01 1.289-01 3.599-01 1.0660-01 1.078-01 2.280-01 2.280-01 3.599-01 1.0660-01 1.078-01 2.280-01 2.280-01 3.599-01 1.0660-01 1.078-01 2.280-01 2.280-01 3.599-01 1.0660-01 1.078-01 2.280-01 2.280-01 3.599-01 1.0660-01 1.078-01 2.280-01 2.280-01 3.599-01 1.0660-01 1.078-01 2.280-01 2.2 | 7.6356-02 6.875-02 1.8107-01 1.825-01 1 |

Figure 3. Sample Output - Continued.

Figure 3. Sample Output - Continued.

XLO XLM XMM

000000	000000000000000000000000000000000000000						00000
-,182316+02 -,196501+02 -,1971696+02		1.19465402 1.19665402 1.19665402 1.196661402 1.18579402 1.18579402 1.18579402 1.18579402	-176,99402 -169425402 -166113402 -168716402 -16801402				242544+01 223269+01 208062+01 197917+01
.2543.0+02 .253908+02 .249729+02	228397+02 2014411+02 20144102 191289+02 193956+02 171068+02	.172853402 .128731402 .109570402 .919680401 .7082959401 .652653401 .6736261	.66436401 .646117401 .628891401 .622039401 .6229407401	.671079+01 .69391+01 .718151+01 .758384+01 .758384+01 .919770+01 .919770+02 .123870+02 .141951+02	17373402 173373402 173373402 172840402 169072402 168620402 163442402	174459+02 175016+02 175016+02 168012+02 159308+02 15715+02 159046+02 159046+02	.15787+02 .153832+02 .148214+02 .142183+02
.259991+02 .245769+02 .230869+02	18 al al min an al al al	125255402 125255402 108070402 947866401 9859301401 756155401 6558155401	.51404-01 .431622-01 .406222-01 .646829-01 .64689-01	120266+02 130072+02 130072+02 13721+02 146955+02 146955+02 149679+02 149679+02	159146402 175691402 193085402 20422402 216314402 219384402 214321402	207764-02 206177-02 206971-02 205082-02 1999262-02 199911-02 189111-02 173866-02	.169258+02 .164949+02 .159686+02 .153117+02 .145%24+02
.213366+02 .204927+02 .195970+02	176278+02 155513+02 155513+02 126811+02 116628+02 105126+02	.55251401 .55024401 .55024401 .816107401 .325861401 .263769401 .263769401	.385275+01 .459139+01 .518153+01 .55679+01 .583082+01	.685322401 .000280401 .100280402 .125636402 .154717402 .164062402 .21009402 .24999402	251190402 250841402 2518410402 251420402 255727402 255727402	2455402 2455402 241229402 235244402 235244402 235994402 220399402 220399402	.205712+02 .197838+02 .190284+02 .183212+02 .176504+02
.344982+01 .308021+01 .263719+01	. 154613401 . 112094401 . 556111-00 . 5164211-01 . 674517-00 . 13498401 . 139980401 . 258856401	. 337270. . 351955+01 . 351955+01 . 310294+01 . 273734+01 . 155613+01	-467672-01 919450-00 193109+01 293047+01 387266+01	.55529+01 .636062+01 .721342+01 .919976+01 .103129+02 .114304+02 .124697+02 .133548+02	145083402 14955402 149552402 150384402 151724402 151724402 152513402 153814402	154022+02 153415+02 152415+02 152758+02 152758+02 150831+02 149226+02 149226+02 143134+02	.131517+02 .123693+02 .115003+02 .105994+02
0000000	000000000000000000000000000000000000000		0000000	0000000	000000	000000 000000 000000 000000 000000 00000	000000.
32.	2 4 4 4 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	655 77 75 80	99 99 99 99 99 99 99 99 99 99 99 99 99	100. 100. 100. 100. 110. 112. 115.	1222 1222 1330 1330 140	59 145.6 60 147.5 62 150.0 64 157.5 64 157.5 65 160.0 67 165.5	172. 172. 175. 177.

Figure 3. Sample Output - Continued.

```
- 199457+01

- 199508-01

- 193522+01

- 193522+01

- 193522+01

- 192508-01

- 192572-00

- 192672-00

- 192672-00

- 192672-00

- 192672-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201961-01

- 201
  . 699287+01
. 7969412+01
. 699768+01
. 699768+01
. 5911255+01
. 5911255+01
. 5911255+01
. 5911255+01
. 5911255+01
. 5911255+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169918+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
. 169618+01
04437 FO 08408 STANFO 08408 FARE 0 08408 FO 08408 FO 08408 FO 08408 FOR 14444 FOR 1444 FOR 14
```

Figure 3. Sample Output - Continued.

								:
.190602+02 .132330+02 .121702+02 .100164+02 .999642+01 .787797+01 .651025+01 .279480+01	-,232006+02	-,303300+02	-,330700+02	359700+02	-,392800+02	430800+02	474000+02	521800+02
353705+02 357563+02 360565+02 350565+02 35317+02 343173+02 341157+02 341157+02 341157+02	ELEVATION	ELEVATION	ELEVATION	ELEVATION	ELEVATION	ELEVATION	ELEVATION	ELEVATION
292756+02 300437+02 307460+02 313715-02 319080+02 3295951+02 3295951+02 331878+02 331878+02	.169900+03 SPL .80508046+02 .66561222+02 .56781729+02	.165970+03 SPL .84504022+02 .6862456+02 .62519719+02	.164460+03 SPL .85599425+02 .69101921+02 .64750934+02	.162250+03 SPL .86650855+02 .64782887+02 .67038012+02	.160350+03 SPL .87622990+02 .69331366+02 .6946199+02 .71042793+02	.157330+03 SPL .88514473+02 .66902869+02 .711+7373+02	.153430+03 SPL .89237861+02 .64441655+02 .73738356+02 .68597191+02	146010+03 SPL
210543+02 .2253643+02 .225324+02 .235324+02 .235792+02 .235792+02 .235792+02 .23618+02 .24318+02 .254818+02	50404 AZIMUTH 50400 PRESSURE • 30746830-04 • 61724728-05 • 19928954-05 • 50246394-05	00+0+ SOUND PRESSURE + 4-807079-0+ - 80634497-05 - 36760025-05	00+0# AZIMJTH SOUND PRESSURE • 55254716-0# • 50112356-05 • 91960707-05	00+04 AZIMJTH SOUND PRESSURE •62544990-04 •79715+45-05 •65207674-05	00+03 AZIMUTH SOUND PRESSURE . 69750150-04 . 756717435-05 . 86041009-05	00+03 AZIMUTH SOUND PRESSURE .77289732-04 .64200964-05 .11214161-04 .97663680-05	00+03 AZIMUTH SOUND PRESSURE .0400202-04 .4635930-05 .14103144-04 .76029282-05	00+03 AZIMUTH SOUND PRESSURE
- 923152-01 - 156681-00 - 319983-00 - 552163-00 - 647071-00 - 451864-00 - 451864-00 - 4673450-01 - 106036+01	.154500+04 SOUND .307 .417 .199	.119700+04 COUND COUND .467 .567 .367 .967	.111400+01. SOUND: .5528. .5528. .501:	.103500+04 SOUND .623 .797 .652	.960000+03 SOUND .697 .756 .860	.890000+03 SOUND 772: 642: 112:	. 626000+03 SOUND . 640 . 483 . 141.	.769000+03
30000000000000000000000000000000000000	RADIUS HANNONIC 2 2 3	HADIUS HARMONIC 2 2 3	HANHONIC HANHONIC 1 2 3 3	RADIUS HARMONIC 1 2 2 3	HADIUS HARMONIC 2 2 3	RADIUS HARMONIC 2 2 3	RADIUS HARMONIC 2 2 3	RADIUS
136 337.5 138 342.5 139 342.5 141 347.5 141 350.6 144 355.5 145 355.5 145 355.6	FIELD POINT	FIELD POINT	FIELD POINT	FIELD POINT	FIELD POINT	FIELD POINT	FIELD POINT	FIELD POINT

Figure 3. Sample Output - Continued.

	-,572800+02	-,622300+02	-,659000+02	-,620000+02	471000+02	-,357000+02
	ELEVATION	ELEVATION	ELEVATION	ELEVATION	ELEVATION	ELEVATION
.6396853502 .61760443+02 .75334465+02 .63968535+02	.140200+03 SPL .89795267+02 .63979433+02 .76709068+02	.128670+03 SPL .89400079+02 .664767+02 .77664767+02	.121800+03 SPL .88941169+02 .69900331+02 .77868108+02 .62971456+02	.513000+02 SPL .84922672+02 .73963460+02 .75559707+02	.266000+02 SPL .82949216+02 .68660622+02 .71412520+02	.174000+02 SPL .79055090+02 .60965327+02 .67866286+02
.86713944-04 .35515691-05 .16948111-04 .45795711-05	.723000+03 AZIMUTH SOUND PRESSURE .8956,9774-04 .4563212-05 .1986,157-04 .2876,8377-05	.667000+03 AZIMUTH SOUND PRESSURE .85458477-04 .75959000-05 .22163404-04 .40051114-05	.659000+03 AZIMUTH SOUND PRESSURE .81181397-04 .90659782-05 .22665380-04 .40629200-05	.662000+03 AZIMUTH SOUND PRESSURE .51113096-04 .14506783-04 .17303360-04	.822000+03 AZIMUTH SOUND PRESSURE .78601208-05 .10790065-05	.103100+04 AZIMJTH SOUND PRESSURE .26010733-04 .3240809-05 .71731905-05 .19797893-05
⊣ณฑ≄	RADIUS HARMONIC 2 2 3	RADIUS HARMONIC D 2 2	RADIUS HARMONIC 1 2 2	RADIUS HARMONIC P	RADIUS HARMONIC 2 2 3 4	HAMMONIC HAMMONIC B B B B
	FIELD POINT	FIELD POINT	FIELD POINT	FIELD POINT	FIELD POINT	FIELD POINT

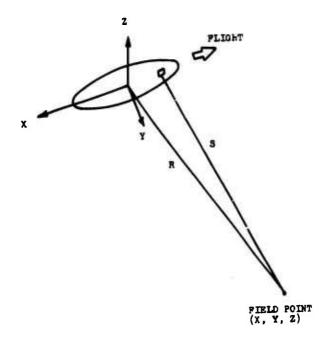
Figure 3. Sample Output - Continued.

:		i			
					,
	LEVEL			LEVEL	
	PRESSURE DECIBELS	8.067#+01 8.4818+01 8.7012+01 8.9054+01 8.9058+01 9.0497+01 9.0497+01 9.0462+01 9.0497+01 9.0462+01 8.9636+01 7.9599+01		PRESSURE DECIBELS	6.7465+01 6.8965+01 6.89620+01 6.8491+01 6.8567+01 7.3457+01 7.3457+01 7.9451+01 7.75451+01 8.1343+01 6.1343+01 6.1343+01
	SOUND PRESSURE DECIBELS			SOUND PRESSURE DECIBELS	
	v			o,	
929		mnnnnnnnnnnnn 0000000000000			
ROTATIONAL NOISE PROGRAM E676	(IN)	-7.3200+03 -7.2260+03 -7.2260+03 -7.2260+03 -7.2260+03 -7.2260+03 -7.2260+03 -7.2260+03 -7.2240+03 -7.2240+03		(IN)	7,2260+03 -7,2966+03 -7,2966+03 -7,2966+03 -7,2966+03 -7,2966+03 -7,2966+03 -7,2966+03 -7,2246+03 -7,2246+03 -7,2246+03
7. P.	IATES			NATES	
IL N019	COORDIN	00000000000000000000000000000000000000		COORDINATES Y	3,00000+03 3,00000+03 3,0000+03 3,0000+03 3,0000+03 3,0000+03 3,0000+03 3,0000+03 3,0000+03 3,0000+03 3,0000+03
ATIONA	OINT	**************************************		POINT	66666666666666666666666666666666666666
P. P.	FIELD POINT COORDINATES Y			FIELD POINT	44488888888888888888888888888888888888
-	×	-1.6600+01 -1.2000+01 -1.2000+01 -1.2000+03 -1.2000+03 -1.2000+03 -1.2000+03 -1.2000+03 -1.2000+03 -1.2000+03 -1.2000+03 -1.2000+03 -1.2000+03 -1.2000+03 -1.2000+03	N	×	1.6800+04 -1.2000+04 -9.6000+03 -9.6000+03 -6.0000+03 -5.6000+03 -2.6000+03 -2.4000+03 -2.4000+03 -2.4000+03 -2.4000+03 -3.6000+03 -3.6000+03
"		7777777777000	II O		77777777777
HARMONIC	FIELD POINT		HARMONIC	FIELD	4704704200004

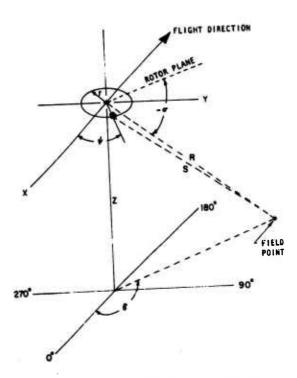
Figure 3. Sample Output - Continued.

```
FIELD X Y Y Z Z COURD PRESSURE LEVEL POLITY COORDINATES (IN) 2 COURD PRESSURE LEVEL POLITY COORDINATES (IN) 2 COURD PRESSURE LEVEL POLITY COORDINATES (IN) 2 COURD PRESSURE LEVEL Z COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S COURD S CO
```

Figure 3. Sample Output - Concluded.



a. OPRONO Coordinates.



b. E3860P Coordinates.

Figure 4. Coordinate Systems for Noise Prediction.

CD COUNT	002 003 004 005 006 006 000	010 011 012 015 016 016 017 018	021 022 023 024 026 026 027 030	0332 034 035 036 038 038 040	042 044 044 045 046 047 048 050 051 052 053
6 7 8	BY G. CAMPE.).OPSI.RR(5).OMEG.CC.NBLADE.MLIMRN.).GAMA.RO.BLADEL.BO.BIC.BIS.PUNCH. 5).GFSET(10.5).WUNIT(5).IBURSI. N(5.5).E3660P.NFT.ANG.KEYI.KEY2. ALCAF(20).OPRUNO.NCH(5).INFERM. 110).NSIATR(5.10).ISEI(5).IREELS.	MDI(4), BHASK(6), NN(435), LIRS, 15), NDZ(14+10+5), XLO(7), XLM(7+40), 16E+10EF, GMARI(288,20), 16E+10EF, GMARI(288,20), 16E+10,20), 1688), BLADES, CARD, TAPE 2(154,10,5), FN(144), CHORD(7), 2(154,10,5), FN(144), GPSI2(41), GPSI3(41)	ATA2), (NN,FN), (TEMP1,CHORD),),AN(31,10,5),BN(30,10,5), ND2(5671),HMAR),(GMARI,AN), HMARI(776),5N),(ND2,02) ND1,01)		
2 3	C MOTON NOISE PROGRAM FOR W. BAUSCH BY COMMON /BKI/ IDD.88.AA.XA(5,5). * MIMOP.XFP(20).YFP(20).ZFP(20). * LSPAN.FROC(30).YFP(20).ZFP(20). * IRS(5).ITRACK(5).FI(5,5).RCHAN(* KEY3.MH: CAPRF(20).THETAF(20). * IREL.NC.NTBDX(5,10).NSTATC(5,1	COMMON /BKZ/ NCYCLE,CYCLES,KU,MOIY(4),BMASK(6),NN(43S),LIRS * KTRACK,KBURSI,KREC,NDI(144,10.5),ND2(144,10.5),XLN(* XMM(7,40),TEMPZ(1),TEMPZ(1),TEMPZ(1),PI,AZMTHZ(144),AZMTHZ * UPRAD,AZRAD,NO,YES,NBLANK,TEE,BEE,DEE,GMARI(288,20), * HAAKI(288,20),XO(20) * COMMON /HEX/ SPLM(10.20),AZMTH3(288),BLADES,CARD,TAPE * COMMON /TEMPUS/ TIME,COUNT * LICHANL(10.5),COSINE(288),SINE(288),BLADES,CARD,TAPE * COMMON /TEMPUS/ TIME,COUNT * UNMENSION DATAL(144,10.5),DATAZ(114,10.5),FN(144),CHORD(7),* * GPSI(7),FSRNN(41),SRNN(41),SRNN(41),SRNN(41),SRNN(41),SRNN(41)	A1) (ND2-D -GPSII) -SN(30-S-S 4-5) 2D) (MARI-CN) ((1) -GMAR) ((MSIAKIEI CALL INPUTA 1F(TCOP.EQ.CAKD) GO TO 199 REWIND 9 REWIND 10 REWIND 11 REWIND 12 REWIND 13 199 LIRS = 0	PI = 3.14159265 UQ = 1=15 IF(185(1).NL.0) LIRS = LIRS+1 I CONTINUE UPRAD = 0PS1*6.28318531/360. AZMTH(1) = 0. AZMTH(1) = 0. AZMTH(1) = 0. UQ 2 1=2.144 AZMTH2(1) = AZMTH2(1-1)+AZRAD Z AZMTH2(1) = AZMTH2(1-1)+2.5 PIZ = 6.283185 AZMTH3(1)=0.

Figure 5. Program Listing - Main.

7 8 CD_COUNT_	055 056 059 060 060 063 064 065 065 066 069	073 074 075 076 078 079 081 082 083 084 085	INPUT. 0888 1089 090 091 092 093 094 094 099 100 101 101 106 106 107
9	DED_AT		OR CARD IN
50.000	OF AZMTH3 HAS BEEN EXCEEDED 8) 4DPRAD 1))	•	TO EITHER ACEPT TAPE OURST.KTRACK
50	60 ANN	FORMAT(1H1,11HAZMTH3(288)) WRITE(6,35)_(AZMTH3(L),L=1,28 BLADES = NBLADE LI = 1,44; CHORUZ(1) = 0, CHORUZ(1) = 1, UO 6 L=2,40 CHORDZ(L) = CHORDZ(L-1)+T1 A LONG LOOP ON BURSTS IS NEXT IF(1DU,NE,1) GO TO 9300 CALL STANT IF(1COP,60,CARD) GO TO 10 HEAD(5,8) IBURST IINE FORMAT(11X,13)	2 2 97
2	11. PRAD)+.001 12. 13. 14. 14. 15. 16. 17. 17. 18. 18. 19. 19. 19. 19. 19. 19. 19. 19	1.11HAZMITH WELADE 1. (AZMITH3 WELADE 1. = 0. 10. 10. 10. TO TO TO 11. GO TO 11. GO TO 12. CARD) GC 12. CARD) GC 13. CARD) GC 14. CARD GC 14. CARD GC 14. CARD GC 15. CARD GC 16. CARD GC 17. CARD GC 17. CARD GC 17. CARD GC	· ·
100	COSINE(1)=1. SINE(1)=0. TI=(F12/DPRAD)+.001 J=1 F(2, 2) IF(J_LE, 288) GO TO 211 WRITE(6,212) *ENT NO. 211 WRITE(6,35) (AZMTH3(L).L=1,2) WRITE(6,35) P12 SIOP AZMTH3(LAZI.) = AZMTH3(LAZI-1 COSINE(LAZI.) = GOS(AZMTH3(LAZI-1 COSINE(LAZI.) = SIN(AZMTH3(LAZI-1 F(1DU.NE.1) GO TO 210 WRITE(6,213)	FORMAT(111,11HAZMTH3(288)) WRITE(6,35)_(AZMTH3(L),L=1,24 BLADES = NBLADE LI = 1,41, CHORDZ(1) = 0, CHORDZ(1) = 1, DO 6 L=2,40 CHORDZ(L) = CHORDZ(L-1)+T1 A LONG LOOP ON BURSTS IS NEX IF(1DU,NE,1) GO TO 9300 CALL STAMT IF(TCOP, EG,CARD) GO TO 10 HCAD(5,8) IBURST STAMT OF BURST TIME FORMAT(11X,13)	A CHOISE I MADE NEXT (OPTION UO 9 I=1.144 UO 9 J=1.10 UO 9 K=1.5 UO 9 K=1.5 UO 9 K=1.5 UO 9 K=1.5 UO 11 IREL=1.IREELS UO 11 IREL=1.IREELS IF(IDU.EQ.1)
1	212	213 210 210 6 7 7 7 9500 6ET	# 6 # 27 X Z X Z Z X Z Z Z Z Z Z Z Z Z Z Z Z Z

Figure6 . Program Listing - Main.

CD COUNT	109 110 111 112	114 115 116 117	118 119 120 121 121 123	124 125 126 127 127	130 131 132 134 134 136	134 138 140 141	144 145 146 147 148	150 151 152 152 154 154	154 159 160 161 162
1 1 2 3 4 5 6 7 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	15 BACKSPACE 10 60 TO 18 16 BACKSPACE 11 15 BACKSPACE 11 17 BACKSPACE 12	BACKSPACE NCYCLE = C THE FIRST CALL ROKU	CALL RDKU(2) KB = KBURST 60 TO 19 C *** THE REMAINING CYCLES IN BURST IBURST ARE READ AND AVERAGED. 20 CALL RDKU(1) IF(KBURST.NE.KB) GO TO 21	CALL RDKU(2) IF(RBURST.NE.KB) GO TO 21 C *** SUBR. UNPACK UNPACKS NN(435) TO FORM NDI(I,J/K) WHERE I=DATA POINT, 19 CALL UNPACK	NCYCLE = NCYCLE+1 CHANNEL LOOP K = NOCH(IREEL) UO 22 J=1, NC = ICHAN(J,IREEL) IF(IDO-1) 234,236,234 IF(IREEL-1) 234,235,234	23 IFILD.EM.1) 234 CONTINUE 235 CONTINUE 235 CONTINUE 237 FORMAT(4113) DO 22 I=1.144 DO 22 I=1.144 DO 21 I=1.144 DO 21 I=1.144		60 T0 28 25 BACKSPACE 10 26 GT 28 26 GT 28 27 BACKSPACE 11 27 BACKSPACE 12 27 BACKSPACE 12 28 GT 28 27 BACKSPACE 12 28 GT 28 39 GT 28 30 G	C *** THE AVERAGE CYCLES ARE FOUND NEXT. K = NOCH(IREEL) LO 29 J=1.K NG = ICHANL(J.IREEL) DO 29 I=1.144

Figure 7. Program Listing - Main.

	163	
TER ROLL OFF CO	166	
UO 30 INTEL=1.IREELS K = MOCH(IREEL)	168	
DO 30 JELYK NC = ICHANE (J. IREEL)	169	
I=1,144	171	
31 FW(I) = DATA2(I)NC.IREEL)	172	
	174	
100 (1) (4) (4) (4) (4) (4) (4) (4) (4) (4) (4	175	
AN(I*L*NC*IREEL) = TEMI(I*I) 32 BN(I*NC*IREEL) = TEM2(I*I)	176	0.0000000000000000000000000000000000000
1F(IDU.NE.1) GO TO 30	178	
=, 13,	180	
1115 MARMONICS FOLLOW // (2X,1PE10.5,12E10.5))	181	
(AN(LINC, IREEL)	183	1
WRITE(6,35) (BN(L,NC,IRE	184	
34 FORMAT (2x.1PE10.3).2010	185	1
CONTINUE	187	September 1
57	188	
NO. = IS. 10x 77HAVE.	189	
KICORRECTED FOR FILTER ROLL-OFF AND ENGR. UNITS)	161	
ALMOCH (INVEL)	192	
NC = ICHALL	190	
AN(1,NC, IREEL) = AN(1,NC, IREEL) + SLOPE(NC, IREEL) + OFFSET(NC, IREEL)	195	
CO 37 INTAME INDP	196	
AN(I+1,NC, IREEL) =	198	
37 BN(INCAREE) = BN(I)NCAREEL)#TI	199	
NO.	201	
	202	-
WRITE(6,39) (BN(I,	203	
59 FORMAT(27X-10(IPE10.3) / (27X-10E10.3))	204	
ORING SURD	202	
TO PRODUCE DIFFERENTIAL PRESS. COEFF. CN(31,5,5), SN(30,5,5) WHER	207	
SUBS. = HARMONIC, SECOND SUBS. = CHORD, THIRD SUBS. = SPAN.	208	
BLADE FITCH HARMONICS, BO.BIC.BIS ARE ALSO CALCULATED.	209	-
1F(ID) 60 TO 240	211	
1	212	
00 239 0=1,5	213	
AKITE COLET	214	

Figure 8. Program Listing - Main.

8 CD COUNT		220 221 222	223 224 225	226 227 228	229	232	234	237	238	242 242 242	שלים בייניים שלים בייניים שלים בייניים	245	248 249	250	252 253	254	256	258	260	262	2664	266	266	270
5 6 7	PRESSURE FOURIER COEFFICIENTS OF THE AVERAGE CYCLES O 41	=.13.11X. 34H*** ROTOR NOISE PUNCHED OUTPUT *	ONICS / S(1PE10.4),2X, 46 TIVELY) / 75HDIFFERENTIAL	IONS AT EACH OF THE 5 SPANS / 66H(MEASURING AND THE BLADE ROOT RESPECTIVELY).)		5HCHORD.12.7X, BHSTEADY= , 1PE10.4)	COEFFICIENTS)	4)) *1»(»])•K=1,MLIMDP)	OEFFICIENTS)	TAPE INPUT) IS ACCEPTED NEXT.			1. IN)	1, J, I), K=1, MLIMDP)	,K=1,MLIMDP)	PRESSURE CYCLES FOR SPAN I CHORD J AZIMUTH K ARE CORRECTED HARMONICS.	INPUT HAS BEEN ACCEPTED (TAPE OR CARD INPUT)							
1 1 2	IAL 60 1	- œ	PITCH	XMONICS FOR 5 CHORD STATIONS X FROM THE LEADING EDGE AND ' C *** SPAN LOOP	C *** CHORD LOOP	I D. CN(1)	19HCOSINE	WRITE(7,47) (CN(K	48) 17HSINE C 47) (SN(K	60 TO 41 C *** CARD INPUT (INSTEAD OF 1 10 READ(5:42) IRURST	READ(5,43)	*	UO 50 J=1,5 READ(5,49) IN.JN.CN(1,JN.IN)	CNCK	NEAD(5,48) 50 NEAD(5,47) (SN(K,J,I),K	AVERAGE DIFFERENTIAL FOUND BY SUMMING THE	ESSUR	0 9301	9301 UO 51 1=1.5 C *** CHORU LOOP	100 51	C *** AZIMUTH (POINT) LOOP	DATALIKACIA) = CN(1, J. I)		}

Figure 9. Program Listing - Main.

COUNT	272 273 274 275 275	277 280 281 282 283 284 285 286	288 289 290 291 292 294 295 296	298 300 301 301 302 303 305 305 305	308 310 311 312 314 315 316 317 318 320 321 322 323 323
5 6 7 8000000	.J.I)*COS(T2)+SN(L,J,I)*SIN(T2) E CYCLES AT INSTRUMENTED BLADE S	STATION. 13//) OR NOT TO CALL THE ACOUSTICS OF THIS PROGRAM.			
2 3 4) = DATA1(K,J,I)+CN(L+1 59HDIFFERENTIAL PRESSUR	DO 53 JELYS WRITE(6,55) I.J. 55 WRITE(6,55) I.J. 53 WRITE(6,56) (DATA!(K,J.!) *K=1.144) 54 WRITE(6,56) (DATA!(K,J.!) *K=1.144) 55 WRITE(6,56) (DATA!(K,J.!) *K=1.144) 56 *** I'HE EOLLOWING INPUT OPTION DESIDES WHETHER 67 *** I'HE EOLLOWING INPUT OPTION DESIDES WHETHER 7 *** I'HE ***	UO 9501 J=1,NHH XLM(1,KK) = 0. 9501 XMM(1,KK) = 0. C *** RADIAL STATION LOOP UO 58 I=1.5 KK = KK+1 JF(IRS(I).E0.0) GO TO 58 LF(NCH(I).E0.5) GO TO 59 NT1 = NCH(I)+2	CHÓRU(1) = 0. DO 6U L=1.5 IF(MAN(I.L).EQ.0) GO TO 60 K=K+1 CHORU(K)=XA(L.1) GONTINUE CHORU(K+1)=1. GPSI(1)=0. UO 61 J=1.144 K=1	U0 62 L=1,5 1F(NCHAN(I)L).EQ.0) GO TO 62 K=K+1 GPSI(K) = DATAI(J.L,I) 62 CONTINUE GPSI(K+1) = 0. CALL AVAUAO(NII.CHORD.GPSI.AREA) 61 FN(J) = AREA*AA 60 TO 63 50 THU 10 = 10. 64 J=1,5 65 L=1,5 65 L=1,5 66 TO 63 67 TO 65 68 TO 67 69 CALL UPSKIE(I+4+NHH,FN.TEMI.TEM2) ALO(KK) = TEMI(I)

Figure 10. Program Listing - Main.

CD COUNT	325.	327 328	329 330	331	533	300 300 300 300 300 300 300 300 300 300	336	338	989	The state of the s	343	##n	0 4 5 U	348	349	350	352	353	355	356	358	359	360	362	364	365	367	368	370	372	373	37¢	376	378
3 4 5 6 7 800000						XLM XMM ,///)	() • (XLM(KK•J) • J=1•NHH) • (XMM(KK•J) • J=1•NHH)			10 10 7	F ANALYSIS					11. The second s				9103			GC2++2)/(288.*SPAN(I+1))		191913181	ERROR 5113)		=1,7200) 1=1,288),HLADES			RN	=1,7200)		
1 2			XLO(KK) = 0. UO 9500 J=1.NM	SOU KENCKKIL) II O.		201 FORMAT(1H1, 11HXLO DO 202 KK=1,7			202 CONTINUE		1) 60 TO		9302 11 = CSPAN-1 11 = 298./11	DELSPN = 11/2. SPAN(1) = 74.		67 SPAN(L) = SPAN(L-1)	FREL	TH = BLADES/(PI+BB)	KEWIND 28	GENERAL STATES OF TO	CELSPAN-2	DO 10005 I=1.J	HSG(1)= PI+(GC1++2=	10005 662=661	60 TO 9103	9100 WRITE(6,9104) LSD2 9104 FORMAT(1H0,11HNTRAN	STOP	9103 WRITE(28) (ND1(I),I WRITE(28) (SINE(I),	END FILE 28	C *** HARMONIC LOOP	CHLIM	REMIND 26 READ (28) (ND1(I),I	C *** RADIAL STATION LOOP	CALL NTRAN(29,10)

Figure 11. Program Listing - Main, Noise Analysis Begins.

CD COUNT	380 382 383 384	366 366 369 390 391 393	394 395 396 396 398 400	400 400 400 400 400 400 400 400 400	411 4112 4113 4114 4115 4115 4110	419 420 421 423 424 425 426 427 429 430 431
5 6 7 80000000	1F(IRS(K).E0.0) 60 TO 69 TD=AA/(2.eRR(K)+BLADEL) *** AZIMUTHAL LOOP DO 99 I=1.144 TI=-TS	T3 = (T2-T1)/40. T6=T1*BLADES*FM COSRN(1) = COS(T6) SIMN(1) = SIN(T6) 16=T2*BLADES*FM COSRN(41) = COS(T6) SINRN(4) = SIN(T6) AZ41(1)=T1	OI = 141		CHORUKKK) = XA(L,K) CHORUKKK) = DATAI(I,L,K) 72 CONIANE CHORUKKK+1) = 1. GPSI(KKK+1) = 0. *** THE MEASURED PRESSURE POINTS ALONG THE CHORD ARE INTERPOLATED ID 41. POINTS CHORUZ(1) = 1. AREA = 1.741.	UO 9307 L=2,40 9307 CHORD2(L) = CHORD2(L-1) + AREA CALL CURVIT(NII,CHORU,GPSI,W,41,CHORD2,GPSI2) UO 73 L=1,41 73 GPSI3(L) = GPSI2(L)*COSRN(L) CALL AVOUAD(41,AZ41 ,GPSI3,AREA) AREA = AREA*T4 9105 IF(LSUZ+1) 9106,9105,9106 9106 CALL NTRAN(29,11,AREA,LSD2) IF(LSUZ+1) 9106,0105,9106 1F(LSUZ+1) 9106,9105,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9105,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9105 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9106 1F(LSUZ+1) 9106,9106 1F(LS

Figure 12. Program Listing - Main.

							•			
7 8 7 COUNT		で の の は か か か か か か か か か か か か か か か か か	N P 3 S 3 S 3 S 3 S 3 S 3 S 3 S 3 S 3 S 3	447 449 449 450 452	453 455 455 455 455	458 459 461 461 462 SSURE PULSE 463		E HARMONICS UP TO 471. 472. 474. 474. 474.	ENTS (
5 4 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	33 HACOUSTIC PRESSURE PULSE COS TERM *10X*15) WHITE(6,2747) COSRN WHITE(6,2747) CHORD WRITE(6,2747) GPSI WRITE(6,2747) GPSI WRITE(6,2747) GPSI	T1, T2 0E13.5)	GF5151L) - GF512(L)#51MKNL) CALL AVGUAD(H1,AZ41 ,GP513,AREA) AREA = AREATT IF(L5U2+1)910U-9107,9108 CALL NTRAN(29:1:1.AREA:L5D2)	CONTINUE CONTINUE IF (LSD2+1) 9100,9200,9201 LALL NTAN(29,10) UO 9109 K=1.5 UO 9109 I=1,144	IF(LSU2+1) 9100,9110,9111 CALL NTRAN(29,2,1,AREA,LSD2) IF(LSU2+1) 9100,9112,9113 GMAR(1,K)=AREA GALL NTRAN(29,2,1,AREA,LSD2)	IF(IDU.NE.1) 9100.9114.9115 HMAR(1.K) = AREA CONTINUE IF(IDU.NE.1) GO TO 75 WRITE(6.76) M WATTE(6.76) M WATTE(6.76) W WATTE (6.76) W WATTE (7.88) W W WATTE (7.88) W W W W W W W W W W W W W W W W W W W	N= 12) L-144) L-144)	THE FOLLOWING SUBR. INTERPOLATES ACOUSTIC PRESSURE PULSE 288 AZIMUTH AND 20 BLADE STATIONS JF(IDD.NE.1) GO TO 9303 CALL CLOCK CALL INTERP. JF(IDD.NE.1) GO TO 79	LAZI,LSPAN 51HINTERPOLATED ACOUSTIC PRESSURE PULSE AZIMUTH STATIONS, 13:1X,17HBLADE STATION SPAN 11HBLADE SPANE, F8.2,10X,21HGMARI(J,I)*HN	INTEGRATION FOLLOWS
1 1	X E E E E E E E E E E E E E E E E E E E	2747 FORMATE 2741 DO 74			CALL SMAR CALL CALL	9114 HMR614KD 9119 HMR614KD 9109 CONTINUE IF (100.NE. WRITE (6.72 X AT EACH (87	C *** THE FOLLOWI C 288 AZIMUTH 75 IF (IDD.NE.1 CALL CLOCK 9303 CALL INTERE	CALL CLOCK WRITE (6.40) 80 FORMAT(1H1: X 13:1X:17H X 13:1X:17H X 13:1X:17H X 13:1X:17H X 13:1X:17H X 13:1X:17H X 14:1X:17H X 14:1X:1X:1TH X 14:1X:1TH	

Figure 13. Program Listing - Main.

																								Control of the Contro		*			7				***************************************																	
CD COUNT	487	488	489	064	164	#65	493	# 1	200	000	127	0 0	200	200	2005	200	200	202	506	201	905	000	510	511	512	513	514	cic	910	518	519	520	521	522	523	524	020 120	250	805	529	530	531	532	533	534	222	0.00 0.40	538	539	240
00					41 11 11 11 11 11 11 11 11 11 11 11 11 1				E DEED NO.												G	2		Andrew Street, Street, St.																						-			1	
7								E, IPE 10.		1021992176	-				100						OK THE SOUND	-		1																						•				
9							STATE OF STA	ANAPPET INCIDATEDA CHATEPET IPELO		1102400211					5)		4				DOUBLE INTEGRATION WHICH VIELDS	9											1		3.1														•	
5	-						ELLI, 12FF (N	The Inc.	21112	500								1HC+ F6.3+1H)			TEGRATION	VMF (M. NFIELD)																												
#0							TARK HAVED	TANGET AND THE	AND GO-CO-CO-CO-CO-CO-CO-CO-CO-CO-CO-CO-CO-CO	ADFS					1900							IELD! AND		į.			* IZ IH)		12	NEXT.											5)									
no	10			03		10 84	DOTATE		THE STATE	(1). III.288). B		2	TO 86	SPAN	IN. 12.1H			N STATIONE . 13.	-		FFFECTS A	UMFCHAN		0 TO 92		AZIILSPAN	1111 IH(+ 13+ 1H++ 1Z+ 1H)		I 1 . JE 1 . LAZ	ON IS DONE	9304							•		. GAVR	46. 13, 20x, E13.	400	10001							
0.0	PSI/2.51+.	(#**b[)	INT LOOP	IELD=1,NFT	MF IELD	M. E. NO. 60	HI. 19METEL			(SINE (1)	2.8	(2.FM.MFTFL)		E	H	1.LSPAN	130X-1 (68	HO. 13HSPAN	90) (61(3)	2X+13;1PE1	OWING LOOP	COMPONENTS	1,2	IF (INTERM.EG.NO) 60 TO 92		93) IILAZI	TI COAN	HOT TANKE	90) (92()	INTEGRATI	L.1) GO TO	¥.	NOT	SPAN-2	TALINDE		I=1.LA71	K+02(I,J+1)	R*RSQ(J)			•	2	11000	FARTI	41.204	LSPAN-1	I=1,LAZI		J=2, IAUDRE
1 1 2	-		FIELD POINT LOOP	DO 83 NE	MIECO = NIEC	IT INTERMISE.	HS FORMAT(1HI. 12	V 0.5 %	STIBBO CON MILE			CALL CUF (2.FM.	IF CINTERM. EG. N	WRITE (6.87)			WRITE	PORMAT(1HO, 13H				_	0.77	IF CINTER	1=K+1	WRITE(6,93) I.L.		WHITE IS.				CALL CLOCK	KING TIECKATION	JAUDRESLSPAN-2	ANEA-0.	000	UD 10007 I=1.L					-	INTRACES OF	CALINAL PARKA					UBI(1)=0.	UO 8821 J=2, IA
			*	*			MS	6	***						87			68	88	3		υ	96			•	2		3	*** 3	92		U KIN					10007			10008	10006			10000	10010	4056			

Figure 14. Program Listing - Main.

```
CD COUNT
  FORMAT(1H0,85 hTHE FOLLOWING ANSWERS ARE OBTAINED BY USING TRAPAZO
1 1 2 3 4 5 6
  9704
```

Figure 15. Program Listing - Main.

595 596 597 598	599 600 601 602 603 604 605	606 608 609 610 611	614 615 616 617 618 619 620	622 624 624 625 626 627 629	630 632 632 633 634 635	6 6 4 5 6 6 4 5 6 6 4 5 6 6 4 5 6 6 4 5 6 6 4 5 6 6 6 4 5 6 6 6 6
XAUAL INTERGRATION ALONG THE BLADE, / X 44HAND SIMPSON S INTEGRATION ALONG THE AZIMUTH. WRITE(6.96) M.NFIELD.TEMPI(1) .M.NFIELD.TEMPI(2) 96 FORMAT(1H0, 44HUMF(1.12.1H, 1.12.3H) =,1PEI0.4,13X, X 44HUMF(1.12.1H, 1.12.3H) =,1PEI0.4,13X,	TATALLES TO THE STATE OF THE ST	X 6H SPLM(*12*1H*,12*3H) =:1PE10.4) SIUDD IF(IDD_NE.1) GO TO 83 WITE(6.9705) 9705 FORMA'(1H0.95 HTHE FOLLOWING ANSWERS ARE OBTAINED BY USING TRAPAZO XIDAL INTEGRATION ALONG THE BLADE AND AZIMUTH WRITE(6.96) M.NFIELD.UTRAP.H.NFIELD.VTRAP UTRAPE(1.7.44121356) #SGRT(UTRAP**Z+VTRAP**Z) UTRAPE(1.7.44121356) #SGRT(UTRAP**Z+VTRAP**Z)	WRITE(6.97) M. WFIELD.UTRAP. H. WFIELD. VTRAP WRITE(6.10004) 10004 FORMAT(1H0. 17H SIMPSON. SIMPSON.) WRITE(6.96) M. WFIELD. USIMP. M. M. FIELD. VSIMP USIMP= (1./1.41421356)*SGRT(USIMP**2+VSIMP**2) VSIMP=20.*ALOGIQ(USIMP/2.9E-D9) WRITE(6.97) M. MFIELD. USIMP. M. MFIELD. VSIMP WRITE(6.97) M. MFIELD. USIMP. M. MFIELD. VSIMP	10011 FORMAT(1HC) WRITE(6,96) M.NFIELD.URING.M.NFIELD.VRING URING=(1./1.41421356)*SGRT(URING**2+VRING**2) URING=20.*ALG610(URING/2,9E-09) WRITE(6,97) M.NFIELD.URING.M.NFIELD.VRING 83 CONTINUE C *** THE FOLLOWING SUBR. PRINTS OUT SOUND PRESSURE LEVELS FOR ALL CALCULATED C *** THE FOLLOWING SUBR.	CALL OUTSPL LE(IDU.NE.1) GO TO 7 CALL CLOCK GO TO 7 STOP LND ADIXG FOR CURVIT (MM. X9. Y9. M. N. X0. Y0.)	CALLING PROGRAM. S NOT USED IN THIS ROUTIN ED LATER FOR A WOPK VECTO SO SO. FOR NOW ASSUME T Y(7), W(1), XO(1), YO(1) IIN 79(1) IIN 79(1)

Figure 16. Program Listing - Main, CURVIT.

CD COUNT	649 650 651 652 653 653 654	656 657 658 659 660 661 663	665 667 668 669 671 672 674 675 677 679 630	682 684 684 685 686 687 690 691 692 693 694 695 696 696 697 698 699 700 700
8		VIT) - LESS THAN TWO POI	D THE COEFFICIENTS.	** (ROOT(1),ROOT1(1),I=1 ION X =, E11.4,3H +, 1.4,7H * T**\$,13H IN S WEN 0, AND 1, WHEN X =, IMAGINARY,(/77X,
2 T	UO 1 IE1,MM X(I) = X9(I) X(I+7) = Y9(I) 1 Y(I) = Y9(I) LF (MM .GE. 2) GO TO 10 LF (MM .EG. 0) Y = 0. LC 3 IE1,N	=	1 60 TO 30 11 60 TO 48 11 (1-1)* TUM1 FEAX(1) + CONST 12 60 TO 64 ECTION FROM WHICH WE NE	LALL CUBL(3), CUBE(2), CUBE, KOOT, ROO LALL CUBLC (CUBE(3), CUBE(2), CUBE, KOOT (I) LF (ABS(ROOT(I)) -1.).GT0001) GO TO 49 LF (ABS(ROOT(I)) -1.).GT0001) GO TO 49 LF (ABS(ROOT(I)) -1.).GT0001) GO TO 60 LF (ROOT(I)).LT.0.) GO TO 50 LF (ROOT(I)).TT.0.) GO TO 50 LF (ROOT(I).TT.0.) GO TO 50 LF

Figure 17. Program Listing - CURVIT.

2) + COEF(2:K,2)*T + COEF(3:K,2)*T*T + 2!*T**3 11		703	
2) + COEF(2;K,2)*T + COEF(3;K,2)*T*T + 2)*T**3 THE PROPER TAPE (UNIT 8,9:10:11, OR 12) THE PROPE TAPE TAPE TAPE TAPE TAPE TAPE TAPE TA		104	
FILIK'2] + COEFIZIK'2]*T + COEF(3JK'2)*T*T + FIG. 18.9.10.11, OR 12) BOKUN BOKUN BOKUN BOKUN (20) TOP. SOPER TAPE (UNIT 8.9.10.11; OR 12) (10) HEADS THE (20) TOP. SOPER TAPE (UNIT 8.9.10.11; OR 12) (21) TOP. SOPER TAPE (UNIT 8.9.10.11; OR 12) (22) TOP. SOPER TAPE (UNIT 8.9.10.11; OR 12) (23) TOP. SOPER TAPE (UNIT 8.9.10.11; OR 12) (24) TOP. SOPER TAPE (UNIT 8.9.10.11; OR 12) (25) TOP. SOPER TAPE (UNIT 8.9.10.11; OR 12) ACKLES TOP. TEAT (10.5) TOP. SOPER TABE (10.5	H0001	705	1
### PROPER TAPE (UNIT 8:9:10:11; OR 12) THE PROPER TAPE (UNIT 8:9:10:11; OR 12) FPE20: SPPE20: SPPE2	2) + COEF(2,K,2)+T	707	
THE PROPER TAPE (UNIT 8,9,10,11; OR 12) -88,44.XA(5,5); UPSI,RR(5); OMEG.CC.NBLADE: MLIMRN, FRICO), ZFP(20); GAAA,RO, BLADELBO BLC,BIS,PUNCH, COP-SLOPE(10.5); OFFSE(10.5); FORFSE(10.5);	21+T++3	708	
## PROPER TAPE (UNIT 8.9.10.11. OR 12) **B8.4A.XA(5.5).0PSI.RR(5).0MG.CC.NBL.DE.M.INRN, FPICO).ZPPICO) 6AMA.RO. BLADE. BD.BLC.BIS.PUNCH, CPP.SLOPE(10.5).0PSI.RR(5).10.15.1CBIS. **D.THETAF(20).ALFAF(20).OPRONO.NCH(5).INTERN, **FI(5.5).NCHAN(5.5).E3660P.NT; ANG.KETI.KEYZ. **D.THETAF(20).ALFAF(20).OPRONO.NCH(5).INTERN, **FI(5.5).NCHAN(5.5).RSZIQQ.10.7STATH(144). **E.CYCLES.KU.NDIV(4).BMASK(6).NN(435).LIRS. **E.CYCLES.KU.NDIV(4).BMASK(6).NU(45).LIRS. **E.CYCLES.KU.NDIV(4).BMASK(6).NU(45).RIRS. **E.CYCLES.KU.NDIV(4).BMASK(6).NU(45).RIRS. **E.CYCLES.KU.NDIV(4).BMASK(6).NU(44).NU(44).NU(44). **E.CYCLES.KU.NDIV(4).BMASK(6).NU(44).NU(44). **E.CYCLES.KU.NDIV(4).BMASK(6).NU(44).NU(44). **E.CYCLES.KU.NDIV(4).NU(4).NU(44).NU(44). **E.CYCLES.KU.NDIV(4).NU(44).NU(44).NU(44). **E.CYCLES.KU.NDIV(4).NU(44).NU(44).NU(44).NU(44). **E.CYCLES.KU.NDIV(4).NU(44).NU(44).NU(44). **E.CYCLES.KU.N	TIME	709	
THE PROPER TAPE (UNIT 8,9,10,11, OR 12) FREATAX (S.5), OPESI RE(S), OMEGE BO. BLC. BIS. PUNCH. FREATAX (S.5), OPESI RE(S), OMEGE BO. BLC. BIS. PUNCH. COP. SLOPE (10,5), OFFSET (10,5), KUNIT(5), IBURST. FILES, NCHAN(S,5), ESBOP, NRT, ANG, KETZ. FOID: NRTATC(S,10), ALRAR(S), OPRONO, NCH(S), INTERN. LE, CYCLES, KU, NDIV(4), BMASK(6), NN(435), LLRS. EC, NOTATC(S,10), NNSTATR(S,10), ISET(S), IRECLS. EC, NOTATC(S,10), NNSTATR(S,10), ISET(S), IRECLS. ES, NULLARK, TEE, BEE, DEE, GMARI(286,20), ES, NULLARK, TEE, BEE, DEE, GMARI(186,20), ES, NULLARK, TEE, BEE, DEE, DEE, GMARI(186,20), ES, NULLARK, TEE, BEE, DEE, TEE, TEE, TEE, TEE, TEE, TEE, T		710	
THE PROPER TAPE (UNIT 8.9.10.11; OR 12) -88.4A.XA(2.5).DFS.1RR(3).OMEG.CC.NBL.DE.MILMRN. COP.S.LOPE(10.5).OFSET(10.5).RUNIT(5).18URSTFE(10.5).OFSET(10.5).RUNIT(5).1RERYFE(10.5).AFFA[-20.0].OFRONO.NCH(5).INTERY10).THETAF(20).AFFA[-20.0].OFRONO.NCH(5).INTERY10).THETAF(20).AFFA[-20.0].OFRONO.NCH(5).INTERY10).THETAF(20).AFFA[-20.0].OFRONO.NCH(5).INTERY10).THETAF(20).AFFA[-20.0].OFRONO.NCH(5).INTERY10).THETAF(20).OFRONO.NCH(5).INTERY10).THETAF(20).OFRONO.NCH(5).INTERY10).THETAF(20).OFRONO.NCH(5).INTERY10).THETAF(20).OFRONO.NCH(5).NCH(4)10).THETAF(20).OFRONO.NCH(5).NCH(4)10).THETAF(20).OFRONO.NCH(5).NCH(4)10).THETAF(20).OFRONO.NCH(5).NCH(4)10).THETAF(20).OFRONO.NCH(5).NCH(4)10).THETAF(20).OFRONO.NCH(5).NCH(4)10).THETAF(20).OFRONO.NCH(5).NCH(4)10).THETAF(20).OFRONO.NCH(5).NCH(4)10].THETAF(20).OFRONO.NCH(5).NCH(4)10].THETAF(20).OFRONO.NCH(5).NCH(4)10].THETAF(20).OFRONO.NCH(5).NCH(4)10].THETAF(20).OFRONO.NCH(5).NCH(4)10].THETAF(20).OFRONO.NCH(5).NCH(4)10].THETAF(20).OFRONO.NCH(5).NCH(5)10].THETAF(20).OFRONO.NCH(5).NCH(5)10].THETAF(20).OFRONO.NCH(5).NCH(5).NCH(5)10].THETAF(20).OFRONO.NCH(5).NCH(5).NCH(5)10].THETAF(20).OFRONO.NCH(5).NCH(5).NCH(5).NCH(5)10].THETAF(20).OFRONO.NCH(5).NCH(5).NCH(5).NCH(5)10].THETAF(20).OFRONO.NCH(5)	OR ROKU, ROKU	711	
### TANGER INC. CONT. 69/10/11 OR 12/10/11 OF 12		712	
FPIZO1.2FP(20): GAMA, RR. BLADEL-BO.BLC. PLINEN. COP. SLOPE (10.5): GAMA, RR. BLADEL-BO.BLC. BL. BU. BU. BU. BU. BU. BU. BU. BU. BU. BU	-	713	
COP-SLOPE (10.5) **OFFST (10.5) **EURST** COP-SLOPE (10.5) **OFFST (10.5) **EURST** FI [5.5) **NCHNN(5.5) **ESBOP **ET** FI [5.5) **NCHNS **ET** FI [5.5) **COLES **COLO **ET** FI [5.5) **COLES **COLO **ET** FI [5.5) **COLES **COLO **ET** FI [5.5) **COLES **COLO **ET** FI [5.5) **COLES **COLO **ET** FI [5.5) **COLES **COLO **ET** FI [5.5) **COLO **ET** FI [5.5	e. 1	714	
FILESS) NCHAN(S.5) EBB60P,NFT,ANG,KET1,KET2. O) THETAF(20) ALFAF(20) OPRONO,NCH(5): INTERM. LID) NSTATC(5.10) NSTATK(5.10) ISET(5): INTERM. ECCYCLES KU,ND(V4): BMASK(6); NN(435): LIRS; ECCNOL(1144.10.5): NNOZ(144.10.5): LIRS; ECCNOL(144.10.5): NNOZ(144.10.5): RN(44): ECCNOL(144.10.5): NNOZ(144.10.5): RN(30:10.5): (SO) (ND2(5671): HMAR): (GMARI:AN): (ND2(5671): HMAR): (GMARI:AN): (LIM:CIM2) LIMI:LIM2)	SPAN-FHOCKSO TCOPECIONS OF THE STATE OF THE	CI)	
10).NSTATC(5,10).NSTATR(5,10).INTER. 10).NSTATC(5,10).NSTATR(5,10).ISET(5).INTER. 10).NSTATC(5,10).NSTATR(5,10).ISET(5).INTER. 10).NSTATC(5,10).NSTATR(5,10).ISET(5).INTER. 10).NSTATC(5,10).NSTATR(5,10).ISET(5).INTER. 10).NSTATC(5,10).NSTATR(5,10).IST(5,10).IST(5,10).ISET(5,1		07/	
LECYCLES ATTC (5.10) -NSTATK(5.10) -ISET(5) -IREELS, LECYCLES ATTC (5.10) -NSTATK(5.10) -ISET(5) -IREELS, EC NO. (144.10.5) -NOZ (144.10.5) -XLO(7) -XLR(7.40) T) TEMP2(7) -TEMP3(7) -PI AZMTH2(144) -AZMTH(144) ES NALLANK -TEE-BEE-DEE-GAMRI(288.20) -ES NALLANK -EE-BEE-DEE-GAMRI(288.20) -ES NALLANK -EE-BEE-DEE-GAMRI(288.20) -ES NALLANK -EE-BEE-DEE-GAMRI(288.20) -EM -EM -EM -EM -EM -EM -EM -EM -EM -EM		777	
LE.CYCLES.KU.NDIV(4).8MASK(6).NN(435).LIRS. EC.NOI(144.10.5).NDZ(144.10.5).XLM(7.40). TEMPZ(7).TEMPZ(7).TEMPZ(144.10.5).XLM(144). ES.NULANK.TEE.BEE.DEE.GMARI(288.20). (20). (1002(5671).HMAR).(GMARI.AN). (HMARI.CN).(HMARI(776).SN) CK.KTRACK).(FBURST;KBURST).(FREC.KREC) (114.5) (114.5) LIMI.LIM2)		/18	
LE.CYCLES.KU.NDIV(4) : BMASK(6) : NN(435) : LIRS : EC.NDI(144.10.5) : NDZ(144.10.5) : XLO(7) : XLW (7.40) : 7) : TEMP2(7) : TEMP3(7) : PI : AZMTHZ(144) : AZMTHZ(144) : (20) : (2	2 4 5	719	
LETTCLESSINGNONDIV(4): BMASKO, NN(195): LIRS; LECTOLS (144.10.5): ND2 (144.10.5): NZLO(7): XLM (7.40): ES: NULANK: TEE BEE. OEE. GMARI(288.20): ES: NULANK: TEE, BEE. OEE. GMARI(288.20): (20) (ND2(5671): HMAR): (GMARI, AN): (HMARI, CN): (HMARI(776): SN) CK: KTRACK): (FBURST; KBURST): (FREC, KREC) LIMI: LIM2; LIMI: LIM3; LIMI: LIMI: LIM3; LIMI: LIM3; LIMI: LI	WCH(5) / LA21	720	
ES, NBLANK, TEFPECTO, SINDZ(144.10.5), XLR(77.40), ES, NBLANK, TEFPECTO, TEMPECTUL, AZMTH(144), ES, NBLANK, TEFPECTO, SHARI(288.20), (20) (144.5) (NDZ(5671), HMAR), (GMARI.AN), (144.5) (NDZ(5671), HMAR), (GMARI.AN), (CK, KTRACK), (FBURST, KBURST), (FREC, KREC) LIMI.LIM2) LIMI.LIM2) LIMI.LIM2) LIMI.LIM2) LIMI.LIM2) LIMI.LIM2) LIMI.LIM2) LIMI.LIM2) LIMI.LIM2) LIMI.LIM2) LIMI.LIM2) LIMI.LIM2) LIMI.LIM2) LIMI.LIM2) LIMI.LIM2)	MAN JEKZ NCYCLE, CYCLES, KU, NDIV(4), BMASK(6), NN(435), LIRS,	721	
7.1 TEMP2(7). TEMP3(7). PILAZMTH2(144). ES.MBLANK, TEE.BEE.DEE.GMARI(288.20). (20) (5). SN(30.5.5). AN(31.10.5). BN(30.10.5). (1144.5) (114.5) (114	TRACK, KBURST, KREC, ND1 (144, 10.5), ND2(144, 10.5), XL0(7), XLM(7, 40),	722	
LIMI.LIM2) LIMI.LIM2)		723	
(20) (144.5) (144.5) (144.5) (144.5) (144.5) (144.5) (144.5) (144.5) (144.5) (144.5) (144.5) (144.5) (144.5) (144.5) (144.5) (144.5) (144.6) (724	
.5).SN(30.5.5).AN(31.10.5).BN(30.10.5). (1144.5) (MD2(5671).HMAR).(GMARI.AN). (HMARI.CN).(HMARI(776).SN) (CK,KTRACK).(FBURST.KBURST).(FREC.KREC) 5761).GMAR LIMI.LIM2) LIMI.LIM2) LIMI.LIM2) LIMI.LIM2) LIMI.LIM2) LIMI.LIM2) .IMI.LIM2) .IMI.LIM2) .IMI.LIM2) .IMI.LIM2)	·	725	
(144.5) (IND2(5671), HMAR), (GMARI, AN), (HMARI, CN), (HMARI(776), SN) (CK, KTRACK), (FBURST, KBURST), (FREC, KREC) (CK, KTRACK), (FBURST, KBURST), (FREC, KREC) (CHI, LIM2) (LM1, LIM2) (LM1, LIM2) (LM1, LM2) (LM2, LM2) (726	
ION NAMPS(219) LENCE (FIRACK, FIRACK), (HMARI, CN), (HMARI, CGMARI, AN), LENCE (FIRACK, FIRACK), (FBURST, KBURST), (FREC, KREC) LENCE (ND1(5761), GMAR) 1 219 217 219 31 217 435 (4.5.6.7.8), I (4.5.		727	
LENCE (FTACK, KTRACK), (HMARI, CN), (HMARI,	6	728	
11321.0 INDICTOR INDI		729	
LENCE (ND1(5761) GMAR) 1.21.N 2.19 2.17 4.35 (WN(I), I=LIM1, LIM2) 9) (NN(I), I=LIM1, LIM2) 9) (NN(I), I=LIM1, LIM2) 9) (NN(I), I=LIM1, LIM2) 9 (NN(I), I=LIM1, LIM2) 9 (NN(I), I=LIM1, LIM2) 9 (NN(I), I=LIM1, LIM2) 1.31 (NNPS(I), I=1, 219) MNPS(I) = AND(NN(I), IM2-2), RMASK(6,1) = AND(NN(I), IM2-2), RMASK(6,1)	CHARL LUST STORY (LINAKI (776) SN)	730	
(1,2),N 1,2),N 1,2),N (1,2)	OLYALENCE (FINACK) FINACK), (FBURST) FINEC, KREC)	731	
1 219 217 435 (4.5.6.7.8),I (1.5.6.7.8),I (1	HOLYALENCE (NDI (5761) GMAR)	732	
119 217 435 (4.5.6.7.8),I (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 13 (NNF(I),I=LIMI,LIM2) 14 (NNF(I),I=LIMI,LIM2) 15 (NNF(I),I=LIMI,LIM2) 16 (NNF(I),I=LIMI,LIM2) 17 (NNF(I),I=LIMI,LIM2) 18 (NNF(I),I=LIMI,LIM2) 19 (NNF(I),I=LIMI,LIM2) 10 (NNF(I),IM2,3) 11 (NNF(I),IM2,3) 11 (NNF(I),IM2,3)	N. (T.T.) OI	733	
217 435 (4,5,6,7,8),I (4,5,6,7,8),I (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 13 (NNFS(I),I=1,219) 14 AND(II) 15 AND(NN(I),IM2-2), AMACK(K))		734	•
217 435 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 13) (NNS(I),I=LIMI,LIM2) 13) (NNPS(I),I=1,219) 14PS(I) 15 (NNPS(I),I=1,219)	١,	735	and a report of the
217 435 (4,5,6,7,8),I (NN(I),I=LIMI,LIM2) 9) (NN(I),I=LIMI,LIM2) 9) (NN(I),I=LIMI,LIM2) 9) (NN(I),I=LIMI,LIM2) 13) (NNS(I),I=LIMI,LIM2) 14) (NNS(I),I=LIMI,LIM2) 15) (NN(I),I=LIMI,LIM2) 16) (NN(I),I=LIMI,LIM2) 17) (NNS(I),I=1,219) 18) (NNS(I),I=1,219) 19) (NN(I),IM2,3) 19) (NN(I),IM2,3)	5	736	
435 (4.5.6.7.8),I (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 1) (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 10 (NN(I),I=LIMI,LIM2) 10 (NN(I),I=LIMI,LIM2) 11 (NN(I),I=LIMI,LIM2) 12 (NN(I),I=LIMI,LIM2) 13 (NNPS(I),I=I,219) 14 (NPS(I),I=I,219) 15 (NN(I),IM2-2),RMACK(K)) 16 (NN(I),IM2-2),RMACK(K))	10 1	137	1
(4,5,6,7,8),I) (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 13 (NNFS(I),I=1,219) 14 NNFS(I) 15 AND(NN(IM2,3) 16 AND(NN(IM2,3) 17 AND(NN(IM2,3)	11 1	738	
(4,5,6,7,8),I (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 13) (NNPS(I),I=1,219) 14 PS(I) 15 AND(INC,IM2,3) 15 AND(INC,IM2,3) 16 AND(INC,IM2,3) 17 AND(INC,IM2,3) 18	X-0X	739	
) (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 9) (NN(I),I=LIMI,LIM2) 9) (NN(I),I=LIMI,LIM2) 9) (NN(I),I=LIMI,LIM2) 1) (NN(I),I=LIMI,LIM2) 1) (NN(I),I=LIMI,LIM2) 1) (NN(I),I=LIMI,LIM2) 1) (NN(I),I=LIMI,LIM2) 1) (NN(I),I=LIMI,LIM2) 1) (NN(I),IM2,3 1) (NN(I),IM2,3 1) (NN(I),IM2,3 1) (NN(I),IM2,3 1) (NN(I),IM2,3 1) (NN(I),IM2,3 1) (NN(I),IM2,3 1) (NN(I),IM2,3 1) (NN(I),IM2,3 1) (NN(I),IM2,3 1) (NN(I),IM2,3 1) (NN(I),IM2,3 1) (NN(I),IM2,3 1) (NN(I),IM2,3 1) (NN(I),IM2,3 1) (NN(I),IM2,3 1) (NN(I),IM2,3 1) (NN(I),I=IM3,IM2,3 1) (NN(I),IM2,3 1) () TO (4,5,6,7,8),I	240	
(NN(I), I=LIMI, LIM2) (NN(I), I=LIMI, LIM2)	11 · (1) NN)	741	
0) (NN(I) · I=LIMI·LIM2) 9) (NN(I) · I=LIMI·LIM2) 9) (NN(I) · I=LIMI·LIM2) 13) (NN(I) · I=LIMI·LIM2) 13) (NNPS(I) · I=1.219) 14NPS(I) 15 AND(NN(IM2-3), RMACK(A)) 16 AND(NN(IM2-3), RMACK(A))		742	
D)(NN(I),I=LIMI,LIM2) 1)(NN(I),I=LIMI,LIM2) 2)(NN(I),I=LIMI,LIM2) 13)(NNPS(I),I=1,219) J=LIMI,LIM2,3 NNPS(I) = ADD(NN(LIM2-2),RMACK(A))		743	200 -
1) (NN(I), I=LIMI, LIM2) 9 (NN(I), I=LIMI, LIM2) 9 (NN(I), I=LIMI, LIM2) 13) (NNPS(I), I=1,219) 14 (NNPS(I), I=1,219) 15 (NNPS(I), I=1,219) 16 (NNPS(I), I=1,219) 17 (NNPS(I), IM2-2), RMACK(K)) 18 (NNPS(I), IM2-2), RMACK(K))	7 10 V WAY 1 1 T 1 T 1 T 1 T 1 T 1 T 1 T 1 T 1 T	## /	
1) (NN(I),I=LIMI,LIM2) 9 (NN(I),I=LIMI,LIM2) 13) (NNPS(I),I=1,219) J=LIMI,LIM2,3 WNPS(I) = ADD/NN(LIM2-2), RMACK(A))		(42	
9) (NN(I),I=LIMI,LIM2) 13) (NNPS(I),I=1,219) J=LIMI,LIM2,3 WAPS(I) = ADD(NN(LIM2-2), SMACK(6))		947	
2)(NN(I),I=LIMI,LIM2) 13) (NNPS(I),I=1,219) J=LIMI,LIM2,3 WNPS(I) = AND(NN(LIM2-2),RMACK(6))		1+1	
13) (NAPS(I), I=1,219) J=LIM1, LIM2, 3 WAPS(I) = ADD(NN(LIM2-2), RMACK(A))	2010 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	877	
J=LIMI, LIM2.3 WNPS(I) = AND (NN(LIM2-3), SMACK(6))		552	
JELIMI, LIMZ, 3 WND(I) = AND(NN(LIM2-2), SMACK(A))	1-1 (TIC-MM) (CT	750	
WAND (I) MAD (II) MAD (II)	(-1 TM1 -1 TM2	16)	
COURT TANK		70/	
COLUMN COLOR		107	

Figure 18. Program Listing - CURVIT, RDKU.

TOUR CD COUNT	757	758	759	The formattee and the format of the control of the	001	761 mm mm m m m m m m m m m m m m m m m m	762	192			IO ZU SPAN		JE ML IMRN.	15.PUNCH.				, IREELS, 772	And the second s	•			<u> </u>	778	779	780			783	784	785	786	787	788	789	190	791	797	707	700	705	702	707	708		ROA	900	802	803	804	805	906	807	808	608	810	
1 1 2 5 6	FREC = ANDINN(LIM2) (BMASK(6))	IF(IDO, FG. 1)	TOTAL TANANTY TANANTY TOTAL TANANTY	THE PROPERTY AND THE PROPERTY OF THE PROPERTY	10 FORMATITHE, 19HINN(1):1=LIMI:LIME; / (EX:10015))	KETUKN	CNA	DOING EAR INTERD	ľ	SUBSCIOUTINE INTEREST	POLATES PRESSURE PULSE HARMONICS FOR UP	STATIONS AND 288 AZIMUTHS.	ŏ			Λ.	_	-	COMMON AND AND AND AND AND AND AND AND AND AN		•.	-	* UPRAD, AZRAD, NO, YES, NBLANK, TEE, BEE, DEE, GMARI (288, 20),		DIMENSION CN(31,5,5), SN(30,5,5), AN(31,10,5), BN(30,10,5)		EQUIVALENCE	1) . BN) . (HMARI.CN)	EQUIVALENCE (NOT (5761) - GMAR)	DIMENSION YO(20)	11=199	12=-801	*** WE FIRST DEFINE THE RADIAL STATION GRID X0(20)	XO(1) = T1	XO(LSPAN) = 1.	K=LSPAN-1	DEL=K	1)F1 = 12/0F1			KKK II S	1 111	1 1	1177	1	NO 2 KEISS	IF(IRS(K),FQ,0) 60 TO 2	2	J(KKK) = GM		TEMP2(KKK) = RR	2 CONTINUE		TEMPI(NOPTS1) = 0.		TEMP2(NOPTS1) = 1.	

Figure 19. Program Listing - RDKU, INTERP.

CO COUNT	811 813 814: 815 816	818 819 820 821 823 824 825 826 826 826 827	833 833 833 835 835 836 837 841 841 841 844	8 8 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	8558 860 861 862 864
1 1 5 6 7 8	CALL CURVIT (NOPTS1,TEMP2,TEMP1,W_LSPAN,XO,YO) UO 3 K=1,LSPAN 3 6MARI(1,K) = YO(K) CALL CURVIT(NOPTS1,TEMP2,TEMP3,W,LSPAN,XO,YO) U	* SIS		SCONTINUE 15(JJ.NE.0) RETURN J=J-2 UO 10 K=1,LSPAN GMARI(J+1,K) = (GMARI(1,K) + GMARI(J ,K))/2. 10 HMARI(J+1,K) = (HMARI(1,K) + HMARI(J ,K))/2. NETURN END HIXG FOR MERGES, MERGES SUBROUTINE MERGES C *** JHS SIRK, PROMITES DIFFERENTIAL PRESSURES, EROM ARSOLITE TOD AND BOTTON	KEAINGS. COMMON /BKI/ IDD.BB.AA.XA(5.5),DPSI.RR(5), COMMON /BKI/ IDD.BB.AA.XA(5.5),DPSI.RR(5), LSPAN.FP(20),TPP(20),ZPF(20),GAMA.RO,BLA LSPAN.FP(C(30),TCD.SLOPE(10.5),OFFSET(10,F),OFFSET(10,F),OFFSET(10,F),TREXCK(5),TRETAF(20),TRETAF(20),ALFAF(20),OFFSELNC,NIBOX(5,10),NSTATR(5,10),NSTAT

Figure 20. Program Listing - INTERP, MERGES.

```
CD COUNT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             C **** CHORD LOOP

UD 2 121.5

C **** CHORD LOOP

UD 2 - 21.5

1SM = 0

1 MEEL = 1 REEL+1

*** NC = 0

1 MEEL = 1 REEL+1

*** NC = 1

*** NC = 0

*** 
1 1 5 6 7 8
                                                                                                                            ပပ
```

Figure 21. Program Listing - MERGES.

CD COUNT	919 920 921 922 924 924 926 926 927 929 931 933	935 936 937 938 939	146 046	945 946 947 947 947 940	952	953 954 955 956	958 958 959	960 961 962 963 964	965 966 967 969 970 971
7 00	OFSRI OFSRI		DFSRI	DFSRI DFSRI DFSRI OFSRI OFSRI DFSRI	DESRI	OFSRI OFSRI OFSRI	DFSRI	DFSRI OFSRI OFSRI	OFSRI OFSRI OFSRI OFSRI OFSRI
5 60	EEL, 1, J	NOT EXCEED HALF INPUTED.							
1 2 3 4 000000	BUC = AN(2,NC BLC = AN(2,NC BLS = BN(1,NC LSMTCH=1 LF(IDU,EQ.1) 60 TO 4 60 TO 4 00 TL K=1,30 CN(K+1,J,I) = B 10 LL K=1,30 CN(K+1,J,I) = B CN(K+1,J,I) = B CN(K	NUMBER OF HARMONICS MUST THE NUMBER OF DATA POINTS NWHEMING(NH,NP/2)	INITIALIZATION AND CONSTANTS.	SP=0. CF=1. NN=2./NP B(1)=0. A(1)=0. A(GHN*3.14159265 C=COS(ARG)	A FOR	UO101=1,NP A(1)=A(1)+Y(1) A(1)=RN*A(1) /2.	MAIN LOOP.	DO 100 K=1.NNH X=C&CP-S*SP X=C&SP+S*CP CP=X U=0.	V=0, COMPUTE RECURSIVE U,S UOZOII=2,NP U=NP-11+2 N=Y(J)+2,*CP*V-U U=V V=W A(K+1)=RN*(Y(1)+CP*V-U)
.	ă	0000	500	j		, 2			C C

Figure 22. Program Listing - MERGES, DFSRIE.

B(K+1)=RNeSPeV	DESRI	973	
KETUKN .	OFSRI	474	
310-310 BOS	DE-SKI	27.0	
SUBROUTINE CUE (N. FM. MFIELD)		577	
17 10	LADE, MLIMRN,	978	
	BISTPUNCH	676	
LSPAN, FROC (30), TCOP, SLOPE (10,5), OFFSET (10,5), KUNIT (5), IBURST,), IBURST,	980	
	EY1, KEY2,	196	
	INTERM.	785	
INCLUSATION STATEMENT OF TO STATEMENT AND STATEMENT OF THE STATEMENT OF TH	DIFTREEFS	702	Commission (a) the commission
MOCHED FLAZI	100	104	
	1.VI M(7.40).	986	
XXX(7-40)-1540-1730-17540-27-17540-37-3-01-42414-37414-37414-37414-37414-37414-37414-37414-37414-37414-37414-3	DATE OF THE OF T	987	
UPRAD. AZRAD. NO. YES. NBL. ANK. TEE. BEE. DEE. GMARI (288, 20).	The state of the s	988	1
×		989	
.M(10.20) . AZMTH3(066	
SPAN(20),		166	
5) + COSINE (288) + SIN		992	
	. ()	266	t t
UNMENTION CHEST STATES OF STANKING STANK STANKING STANKING STANKING STANKING STANKING STANKING STANKIN		\$66	
9		2773	
		946	
		966	
		666	-
T5=PI/180.		000	
	210.00	100	100000
-		005	
8		200	
		*00	
WALLEGO J. COAM	i	500	
		900	
	经有权 指於	100	
		000	
		010	
7		110	
DO 1 1=1.LSPAN		012	
AZIMUTH LOOP		013	
DO 1 JEINLAZI		014	
PED METER CHASS	+ ITPPINETELDI-SPANILLI	210	
v	(L) 1=TS	910	
		018	
COSB = COS(B)		610	
T4 = FM+BLADES+(AZMTH3(J)+(S+OMEG+T1)/CC)		020	
*		021	
		022	
T4= (FM+BLADES+OME6/(CC+S++2))+T1	ACT CONTRACTOR OF THE PERSON NAMED IN CO	023	
MICHEL STREET OF THE COMPANY TO STREET THE STREET TO STREET TO STREET THE STREET THE STREET THE STREET THE STREET THE STREET THE STREET STREET THE STREET ST	II / JNI II	100	F

Figure 23. Program Listing - DFSRIE, CUE.

	92(Jr.I) = 91(Jr.I) = (GMARI(Jr.I) = (-T2/See3 - Te=T3) +	027
~	Š	028
	JF(1.67.2) 60 TO 1	030
	_	031
	WRITE(6,4) I.J.MFIELD FORMATCHD.6113)	032
1		0.34
	K B1(3:13:92(3:1) 66 TO 1	929
N	* (GMARI	037
٦.	X MMARI(U: 1) + (-12/5++3 - 14+13))	038
1	KETURN	040
	ENG.	041
9719	FOR ELECTRIC SECURAL PLOST PROPERTY OF THE PRO	200
	K1/ ID0	***0
-	-	540
-03	COP, SLOPE (10,5), OFFSET (10,5)	9#0
-	KENNICH FINGEN (1977) THE THE CONTRACT OF THE	740
		0 0
*		020
ľ		051
	* XMACK, KBUKS MKEC, NO. 1 144, 10,5) MCC. 144,10,5) ALU. MCC. 144,10,5 ALU. MCC. 144,10,5 ALU. MCC. 144,10,5 ALU. MCC. 144,10,5 ALU. 053	
•		450
	THANK (2005) ON THANK (2005) ON THANK (2005)	055
•	SPAN(20)	020
ľ	.5) . COSINE (288) . SINE (2	058
	DIMENSION CN(31,5,5), SN(30,5,5), AN(31,10,5), BN(30,10,5),	029
	GEAR (144.5) TAMAR (144.5)	090
40	(ND2 (S671) - HMAR) - (GMART-AN)	262
٦	. (HMARI, CN).	063
20	EQUIVALENCE (NDI(5761);GMAR);(NDI,01)	990
-	T STATION IS	990
	5) /1,2,3,4,5	790
NCH I	C NCHANILLO IS AN ISTRUMENTED CHORD STATION COUNTER O FOR EACH RADIAL STATION I	990
1	10.(2.1)	070
^	2	071
35	I=CHORD STATION.	073
*	DATA (XX4(1.4),1#1.5),4#1.5)/ .042,158,300,600,910,	976
	6001.9101	076
CH	O. OF CHORD ST	77.0
7.70	UDATA (NCHILI)-11-15/5-15-15-15/	076
-	é	

Figure 24. Program Listing - CUE, BLODAT.

*** ***	11 CHORD STATEON 3. 0884
X .1.1222355222. X .1.1222355222. X .1.1222355222. DATA (NDIV(I),I=1.4)/0 001 030 000 000. 0 000 001 X 0 000 000 001 000 0 000 000 000 000 00	
11.11.22225322 14.170 001 030 000 000. 0 000 001 0. 0 000 777 000 000. 0 000 000 7. 0 777 777 000 000. 0 000 000 1 APL/4HTAPE/.CARD/4HCARD/ /1HT.1HB.1HD/	A STATE OF THE PARTY OF THE PAR
X 0 000 000 001 000. 0 000 000 000 001/1/HMASKIII/ X 0 777 000 000 000; 0 000 777 000 000; 0 000 00	
X 0 777 000 000 000 0 000 777 000 000 0 000 000 X 0 000 00	
DATA TEE BEE DEE / JHT LHB I HD/ END	7 000 088
DATA TEE-BEE-DEE /1HT.1HB.	
	760
	260
SUBBOUTINE IMPUTA	000
THIS SUBR. RECEIVES CARD IMPUT	960
COMMON /BKI/ IDD.88.AA.XA(5.5),DPSI,RR(5)	•
TCOP. SLOPE (10.5) . OFFSET (10.	ADEL: BURBLE BIST PONCH.
	v.
* IREEL.NC.NTBCX(5,10),NSTATC(5,10),NSTATR(5,10),ISET(5),IREEL	T(5), IREELS, / 101.
* KTRACK, KBURST, KREC, NO1(144,10-5), ND2(144,10-5), XLO(7), XLM(7,4C)	
. XMM(7,40), TEMP1(7), TEMP2(7), TEMP3(7), PI.AZMTH2(144), AZMTH(144)	
* HMARI (286,26), x0(20)	107
* SPAN(20).	601
5) COSINE(288) SINE(288) BLA	
	AN),
* (GRANI(1551):BN): (HMANI:CN): (HMANI(776):SN): (ND2:02) DIMENSION CN(31.5.5): SN(30.5.5): AN(31.10.5):RN(30.10.5)	112
*	
	115
EQUIVALENCE (NDI(5761), GMAR), (NDI, 91)	116
1 FORMAT(1346, A2)	118
	119
(46, A2)	
(EAD(5,3) BB, AA,BL	
S FORMAT REFLES TOP PONCH IN ENM IDO	122
60 TO 45	
DO 100 1=1,5	125
DO 100 JUL 1.10	126
100 NSTATR(19.4J) = 100	128
DO 16 J.E.	129
MEAD(5.4) IREEL. ITRACK(IREEL). ISET(IREEL). KUNIT(IREEL)	130
X IREEL, ITRACK (IREEL), ISET (IREEL), KUNIT (IREEL)	
77 FORMAT(5113)	133

Figure 25. Program Listing - BLODAT, INPUTA.

	135
(IREEL, NC)	136
S SLOPE (NC 18EEL) FOF SET (NC 17 SEL) NC NO	137
(IREEL)+1	139
	140
¥	141
IF (NCEND.E.G. 0) 60 TO 6	142
KEAD(5,7) (FROC(J) - J=1,30)	241
3.1.2X)	145
	146
IF (E3860P.WE, YES) 60 TO 9	148
KEAD(5,10) ANG, NEWL KEY1, KEY2, KEY3	149
FORMAT(E7.0.4(2X.12))	150
IF(E3860P.NE,YES)60 TO 12	152
READ(5,13) CAPRELLI, THETAE(1), ALFAE(1), XFP(1), YFP(1), ZFP(1)	153
FORMAT(SE10.1,20X,3E10.1)	154
HEAD(5,14) XFP(1),YFP(1),ZFP(1)	156
FORMAT(50X, 3E10.1)	157
CONTINUE NOW THE INDUIT IS DRINTED OUT.	158
AA.CC.BLADEL, OME	160
SCHEERO TWIST BLADE STA. (IN) = . E10.4. // SX.	191
HORD (IN) = .E10.4, 8	163
(IN/SEC) = ,E10.4 // 2x,28HBLADE LENGTH (IN) =	164
4 35HKOTOR ROT. SPEED (RPM) = ,E10.4 // 48X,35HAZIMUTH	155
(DEG) = .E10.4 / 2x, 28HBLADE T	167
61N) = #E10.4) watte(4.31) Nai Ant. 1000. Milland. Dilach. M. 100N. Intern. 1001. 1000.	168
ER OF BLADES, 32X.	170
. 2HE . A. // 2X, 49HNO. OF HARMONICS TO REPRESENT	17.1
255URE CYCLES = , 13, 14x, 35MPRESSURE MARMONIC PUNCH OPTION =	:72
. AI // 2X. 28HNO. OF ROIGH NOISE HARMONICS, 20%; 2Hm . 12, 14X.	173
4 CONTINIENTALIS COLLONS 124 CAR 12 // CAR SANOT INTE	174
()	176
IF (TCOP, E9, CARD) 60 70 46	177.
DO 22 INEC	178
ICL NO. = . II. 4X.12HTRACK NO. = .	180
12. 4x, 24H	187
JHCHARMEL, 24X, SHSLOPE, 14X, GHOFFSET)	162
DO 22 121,K	184
NC = ICHANL(I.IREEL)	185
#KITE(6,24) NC.NTBOX(IREEL,NC),NSTATC(IREEL,NC),NSTATR(IREEL,NC),	186
T SECURITION TO LIGHT WAS THEFT.	73

Figure 26. Program Listing - INPUTA.

SLOPE(NC.IREEL) = SLOPE(NC.IREEL)/256.	189
	190
	161
Ξ,	192
LICE DAT LOTH KER. CORK. PALION // 1	193
	194
TOTAL TERROR TO THE PROPERTY OF THE PROPERTY O	ck!
FORMAT (10x 12 - 13x - 19E 11 - 4 - 25x 12 - 13x - 19E 11 - 4 1	190
26 CONTINUE	198
WRITE(6,27) E3860P, OPRONO, NFI	199
62HOPTION TO USE PROGRAM E386 (200
2H= , A1 // 2X, S9HOPTION TO USE ROTOR NOISE	201
RESSURE PULSE) .IIX. 2H= . AI // 2X. 19HNO. OF	202
¥	203
YES) 6	204
MALIE (D.Z.) ANGINHIS BETTISETZINETS	205
LA TOWNSTON STATEMENT OF INTERNATION USED IN ESSES (DEG.) H. F.	206
1 TAIL COUNTY AT BITH LYMN THROWNING BY LEIGHT BY LEE FIZECANDING TO:	207
TATE TO DETAILS AND THE PARTY OF THE PARTY O	500
19	202
ERITE(6.36)	211
36 FORMET 25% 17 FLAG FIELD POINTS, 32% 24MOTOD NOTCE FIFT DOTANT	213
X,2HFP,7X, 6HR (FT),7X, 24HTHETA (DEG) ALPHA (DEG).	213
2, 7X, 6HX (IN), 7X,6HY (IN),7X,6HZ (IN) /)	214
	215
60 IF(E3860P.NE.YES) 60 TO 30	216
IRLTE(6, 57)	217
	218
A COEST	219
SO DESTRUCTION	220
FORMAT! 74X. 24HR	222
1): TAIBHY (IN): TX: 6HZ (IN) /)	223
	224
FS.A	225
WRITE(6, 39) I.CAPR	226
ST COMMAN STATESTAN SISTEMBERON 227	
THE COL COLOUR PRESENTATION OF THE PRESENTATIO	228
WRITE (6.39) T.CADD	222
<u>80 TO 32</u>	241
	232
FORMAT (61X; 12,2X;	233
32 CONTINE	234
E LONG	235
FOR LINDACK	236
CHARGITANE IMPACE	25/
** THIS SUBR. UNPACKS A CYCLE NN(435) TO FORM THE ARBAY ND:(144.10.TDEF)	
WHERE THE FIRST SUBSCRIPT REPRESENTS AZIMUTH, A	240
REPRESENTS CHANNEL NO.	
	74.7

Figure 27. Program Listing - INFUTA, UNPACK.

	### ### ### ### ### ### ### ### ### ##	243	247	248	249	250	257	253	254	255	256	257	25.0	260	261	262	263	265	266	267	269	270	271	273	274	275	277	278	279	280	282	283	285	286	287	000	290	291	292	295	295	700
	OP'SLOPE(10'5),OFFSET(10'5),KUNIT(5),IBURST, FIRST, NCHAN(S.E),FREECOD,NET,ANG,KEV:KEVS	THETAF(20) ALFAF(20) OPRONO NCH(5) INTERN	0) NSTATC(5,10) NSTATR(5,10), ISET(5), IREELS,		CLES, KU, NDIY (4), BMASK (6), NN (435), LIRS,	C.NOI(144,10,5),NO2(144,10,5),XLO(7),XLM(7,40),),TEND2(7),TEND3(7),DI,AZNTH3(444,AZNTH),AZNTH	S. NET ANK TIFF BEFF CIFF GRADI CORE COLL		(ND2(5671) HMAR) (GMARI'AN)	(HMARI, CN) , (HMARI (776) SN)	5)+SN(30,5,5)+AN(31,10,5),BN(30,10,5),		/000							to design the second of the second se					60 TO 1								The state of the s	.GT.0) RETURN	FAILENDID INCEL!(NDININATEL)/RE1010) FORMAT(1HO, GHIREEL=/13/10X)	/2x,10113)		The second secon		2), DEL(7,2), DIST(7), A(7, 8), Q(7,2)		
P(20)	FICOP	KEY3. NHH, CAPRF (20) . T	0	NOCH(S) LAZI	COMMON /BKZ/ NCYCLE, CY	KIRACK, KBORSI, KREC, NI XMM (7, 40), TFMP1 (7), TF	DPRAD AZRAD NO YES NE	HMARI (288, 20) , XO(20)		* (SMARI(1551), BN), (HM)	DIMENSION CN(31,5,5)	EQUIVALENCE (ND1/5741).GMAR	UATA SIN/O 400 000 000	_	WRITE(6,6) NN	FORMAT (2X, 10013)	AZIMUTH POINT LOOP	UO 1 I=1.144	- 274	TANK LYOF		ADAGMI OT	5	N10 = N10-1	J.EG.3.AND.K.GT.2)	1 - 2C - 1 - 2C - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	GO TO 2	" NI*NDIA(NIO)	NI = NICHDIVILI	v2=AND(V2,SIN)		AFTIVE OF NITUTE	1 (3)	IF (IDD. NE. 1. AND. NCYCLE	OHIREEL=	10, IREEL)			FOR PAKAMITAKAM SUBBOUTINE DARAM IN. 6	- 0	COMMON /COTAN/ T()	

Figure 28. Program Listing - UNPACK, PARAM.

```
8
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 A(1,2) = 2.* DIST(1) + DIST(2)*1.5

A(1,2) = 2.*(DIST(1) + DIST(2))

DO 33 J=1.2

W(1,1) = 3.*(DIST(1)/DIST(2)*DEL(2,J)+DIST(2)/DIST(1)*DEL(1,J)) -

W(1,1) = 3.*(DIST(1)/DIST(2)*DEL(2,J)+DIST(2)/DIST(1)*DEL(1,J)/2.).

* DIST(2)* T(1,J)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   9(I,J) = 3.*(DIST(1)/DIST(I+1)*DEL(I+1,J)+DIST(I+1)/DIST(I)*DEL(
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             +DIST(N1 )/DIST
+DIST(N1 )/DIST
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          FOR TRIDAG, TRIDAG, TRIDAG, S.KI, Z.)
SUBROUTINE TRIDAG, A.G.KI, Z.)
UIMENSION A( 7,8), G(7), Z(7)
FORMAT (10%, 50HT=0. .OR. 5=0. IN TRIDAG. CANNOT DIVIDE BY S.OR.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    DO 45 I=1.NI
COE(4.1.J)=-2.*DEL(1.J) + DIST(1)*( T(1+1.J)+T(1.J) )
COE(3.1.J)= 3.*DEL(1.J) - DIST(1)*( T(1+1.J)+2.*T(1.J) )
COE(2.1.J)= DIST(1)*T(1.J)
COE(1.1.J)= P(1.J)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      L 27 4(N2, J) = 1.5*(DIST(N2 ) + DIST(N1 ) + 2. (N2 ) + 4(N2 ) + 3.*(DIST(N2 ) / DIST(N1 ) + DEL(N1, J) + 4(N2 ) + DEL(N2, J) - DIST(N2 ) + T(N, J) + T(N2 ) + T(N2 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 ) + T(N3 )
                                                                                                           NZ = N-2

NJ = N-3

NU=N2

1G0 = 2

UO 15 I=1*N1

UO 10 J=1*2

UO 20 I=1*N

UO 20 I=1*N

UO 20 J=1*N

NO 30 J=2*N

NO 30 J=1*N

NO 30 J
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             CALL TRIDAG(A(1,2), G,NO,T(2,J))
T(1,J) = 1.5/DIST*DEL(1,J) - .5*T(2,J)
T(N,J) = 1.5/DIST(N1)*DEL(N1,J) - .5*T(N1,J)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        SOLVE THE TRIDIAGONAL MATRIX EQUATION
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                PURPOSE
TO S
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   07
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          22
```

Figure 29. Program Listing - PAHAM, TRIDAG.

351	352	ESC	# #	* *	999	300		*6*	090	190	790	197 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	CBC - + +	790		SINGLE ELEMENT.	372 DIAGONAL C CENTEDED ON THE BRINCIOA!	TRIDIAGONAL MATRIX	ATION. VECTOR OF LENGTH KIL	MATRIX A.	COLUMN) OF LENGIN KI.	626	000 18E	382	383	300°C	2 9 9 P P	782	388	389	165	392	393	468	395	396	CAS.	060 K	PROCEEDING BACKWARDS 400	10h-	NOT:
	* * *	* * * * * * *	*		* 1		*	*	* *	****			***	*** *********	FOR THE SOLITIONS 2. WHERE GALLS	CONSIST OF A SINGLE ELEMENT	DESCRIPTION OF PARAMETERS A MATRIX WHOSE THREE DIV	DIAGONAL BECOME I	RIGHT HAND SIDE OF	1 NUMBER OF ROWS IN	Z == SOLOTIONS/ VECTOR (COL	TOTAL TRANSPORT OF THE COST OF		A(1-1)		(5 .E.W. U.) 60 10 23 6(1)/5		= K1-1	0 1=2,K2	A(1,1-1) A(1,1)	A(I, I+1)	UENOM = T*D+S	(G(I)-C+1)/DENOM	-K/DENOM	CONTINUE Simplify:	A(K1.K1.) A(K1.K1-1)	Z(K1)=(G(K1)-T*C)/(T*D+S)		CALCULATE OTHER SOLUTIONS, PROC	09 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

Figure 30. Program Listing - TRIDAG.

÷								
COUNT	406 406 407 408	69121	4114	6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	426 428 429 430 430	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	### ### ### ### #### #################	4449 4449 4449 4449 4449 4449 4449 444
G 6 7 8 CD			· ·	OH W+ (V) #0+(V##K) #4+(O##K)				
1 1 2 3 4	DO 20 I=2,K3 U = K1-I S = A(J+1,J+1) K = A(J+1,J+2)	1 = A(J+1,J) IF(T = EG. 0.) GO TO 25 Z(J) = (G(J+1)-S*Z(J+1)-R*Z(J+2)]/T 20 CONTINUE Z(1) = (G(1)-A(1,2)*Z(2))/A(1,1)	SETURN 25 WRITE(6,1) RETURN END GIXG FOR CUBIC, CUBIC CUBIC, CUBIC CUBIC, CUBIC CUBIC, CUBIC CUB	UIMENSION 90 UIMENSION 90 UO 220 I=1,3 ROOT(I)= 0. 220 KOOTI(I)=0.	# 1 1 PJ	SMALLC = 84 + A27 IF (SMALLC)14 , 1 ,5 1 XA=SMIT (-AD3) IF (SMALLB) 3,4,4 3 XA=XA 4 NOOT(1) =XA-P3 HOOT(2) = ROOT(1)	n	6 B16A1 =-(1-B16A)** POWER). 60 T0 9 7 616A1 = 0. 60T0 9 8 B16A1 = (B16A) ** POWER 9 1F (B16B) 10 , 11, 12 10 B16B1 =-((-B16B) ** POWER) 60 T0 13 11 B16B1 = 0. 60 T0 13 12 B16 B1 = (B16B) ** POWER 13 13 AB = B16A1+B16B1

Figure 31. Program Listing - TRIDAG, CUBIC.

KOOT (1) F A8-P3 KOOTI(1) E 0.	459
(S) = -A	461
KOOT (3) =: KOOT(2) KOOTI(2) =: SGRT (3,)/2, *(BIGA1 - BIGB1)	462 463
= - ROOTI (2)	19th
14 HAD = 57.2957795	466
CON = 120./ RAD	467
(SMALLB) 15,	694
	470
60 TO 18	472
16 PN3 = 30./ RAD	473
17 COT = 180, ZRAD	*
CP:: -1.	924
- 84 /A27	477
COSTIL TOTAL DEFAULT	478
T = ATAN (XK/	690
£	191
00 20	432
AK = A3+ A3	1801
ANGLE =PH3	485
DO 21 1 = 1,3 ROOT (1) = AK # COS (ANGLE)-P3	486
ANGLE +CON	888
22. KETUKN	489
DIXG FOR OUTSPL, OUTSPL	164
SUBROUTINE OUTSPL	492
COMMON YORLY IDDIODS ANY MAINT STATES OF STATE	767
LSPAN, FROC(30), T	495
* IRS(5), ITRACK(5), FEI (5:5), NCHAN(5:5), EUSGOP, NFI, ANG, KEYI, KIN, KEYI, KIN, KIN, KIN, KIN, KIN, KIN, KIN, KI	965
IREEL, NC, NTBUX (5, 1	498
	661
* KTDACK.KRUBAT.KBFC.NOT.THEL.10.51.NOT.THEL.10.51.XI.0.73.XI.	500
	502
UPRAD, AZRAD, NO. Y	503
* TEAKI(288,20),X0(20) COMMON /HX3/ COIM(10,20),APMIHA(288),	500 505
SPAN(20)	909
INE (288)	507
# GMAK(144.5).HMAK(144.5)	509
EQUIVALENCE	511
* (GMAKI(1991), GN), (HMAKI, CN), (HMAKI(776), SN), (NDZ, GZ)	512

Figure 32. Program Listing - CUBIC, OUTSPL.

1				3							de la martin de la company que and man de descriptions of the professional section of the sectio						Anne delle Minime. Del 0											andere er er erskemmen errend zuder deutlem mitte für für der die der
CD COUNT	513	516 517 518	520	522	525 525	527 528	529 530	532	533 534	535 536	537	683	541	543	544	246	543	549	551	552	554	555	557	559	560 561	562	264	566
6 7 B		/ 8ו	COORDINATES (IN), 10x,14x,14x,14Y,				ì	***		ı		GE INTERPOLATION						[X(2)*+2]-(X(1)**			· · · · · · · · · · · · · · · · · · ·		1	31	•X(K+1)))			[Ä(K+1)**¢)=!Ä(h!
5 4	761), GMAR), (ND1, 01)	9HROTATIONAL NOISE PROGRAM E676	11X, 28HFIELD POINT),YFP(J),ZFP(J),SPLM(I,J) 3(5x,1PE10.4),15x, 1PE10.4)		40NIC =,13)		T J.XFP(J),YFP(J),ZFP(J),SPLM(K,J)			(N)X)Y,AREA) RAGED QUADRATICS BASED ON LAGRANGE		(1)-x(3)))	#(X(2)-X(3))) #(X(3)-X(2)))) + T2#(X(1) +X(3)) + T3#(X(1) +X(2)) 2#X(1) #X(3) + T3#X(1) #X(2)	##3 -{X(1) ##3) +(B2/2, #(X(2) ##2] -{X(1)				(X(K)-X(K+2))))*(X(K+1)-X(K+2))))*(X(K+2)-X(K+1))		DZ==(]#(X(K+1)#X(K+Z))#TZ#(X(K)#X(K+Z)}#TZ#(X(K)#X(K+1)) CZ=T]#X(K+1)#X[K+2)#TZ#X(K]#X(K+Z)#TZ#X[K]#X(K+1)			(X(N+1)++5)-(X(N)++5))+(B/Z-)+((X(N+1)++Z)-(X(N)
1 2 3	EGUIVALENCE (ND1(5761),6 Harmonic Loop Do 1 I=1,mlimm,2	OI FD	FORMAT(1HO, BX, SHFIELD, 16X, 20HSOUND PRESSURE		XFP(J	IF(I.GE.MLIMRN) GO TO 7	WRITE(6,6) K FORMAT(1H2 / 8X+10HHARMONIC	WRITE(6.3) FIELD POINT LOOP	5 S	CONT INUE RETURN				T1=Y(1)/((X(1)-X(2))*(X(1)-X(3)))	12=Y(2)/((X(2)-X(1))*(X(T3=Y(3)/((X(3)-X(1))*(X(A2=T1+T2+T3	B2=-(11*(X(2)+X(3))+T2*(C2=T1*X(2)*X(3)+T2*X(1)*	AREA=AREA+(A2/3.)	N2=N-2	UO 101 K=2.N2 A1=A2		TI=(K)/((X(K)-X(K+1))*(X(K)-X(K+2)))	12=7(K+1)/((X(K+1)-X(K)) 13=7(K+2)/((X(K+2)-X(K))	A2=T1+T2+T3	GZ=T1*X(K+1)*X(K+2)+T2*)	A=(A1+A2)/2. B=(B1+B2)/2.		**2))+C*(X(K+1)-X(K))
	A #	์ เ	٠ <u>,</u> ×٠	(* * * · ·	3 U	~ %	9	***		J I .	9XI0	<i>J</i> , ~	_ ¬	- ~	,- -		·		4-	_ ¬		1 	-					1

Figure 33. Program Listing -OUTSPL, AVQUAD.

CD COUNT	568	570 571 572	573	575 576	577 878 570	590	1001 2002	7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00	586	588	589	592	594	595 596	598	009	602	603	605	209	609	610 611	612 613	614 615	616	618	620
1 1 2 3 4 5 6 7 8	AKEATAREA+(A2/3。) + ((X(N)++3)-(X(N-1)++3) \+(B2/2。) + ((X(N)++2)-(X(N-1)+2) \+(B2/2 + (X(N)+X(N-1)) \+(B2/2 + (X(N)+X(N)+X(N-1)) \+(B2/2 + (X(N)+X(N)+X(N)+X(N)+X(N-1)) \+(B2/2 + (X(N)+X(N)+X(N)+X(N)+X(N)+X(N)+X(N)+X(N)	E386RN			# INSID * LINACR(5)**TIO**D!*NCHAN(5*5)*R5B6OP*NFT*ANG*REYI*REYZ* # KEYS*NHH*GAPF(20)*THETAF(20)*AFFAF(20)*DPRONO*NCH(5)*INTERM* # IRFE*L*NC*NTBDX(5*10)*NCTATC(5*10)*NCTATP(5,10)*TAFFTA;	COMMON ARXX NOTE: FOR FOREIGN FOR THE BRACK AND AND ARX AND ARXX NOTES AND ARXX N	* KIRACK * KOURST.KREENOILING***********************************	* AMM.(**U), EMTI(7), EMZ/7), EMZ/7), EMZ/7), PI,AZMIHZ(144),AZMIH(144), * DPRAD,AZRAD,NO,YES,NBLANK,TEE,BEE,DEE,GMARI(288,20), * HMADIZAR,JOI,*YO(30)		SUIVALENCE	551), BN), (HMA CE (NO1(5761)	DIMENSION 1 V25(721), V251(721), PSI(721), PRAD(721)	HEAD FLT. COND. PARAMETERS AND BLADE SECTION LOADING, PRINT SAME.	KBNENBLADE EGITVALENCE	X (CHAN, MLIMRN), (SOS, CC), (BD1, BD), (B1, B1C), (B11, B1S), (G, GAMA), X (NHAN, MLIMRN),	•	6ATCZ=BIC	GAICOEBIS	GATC5=OMEG 505 = 505/12.0		00 730 I=1,5	JE(185(1), E0.0) GO TO 730	K(J)=KK(I)+BLADEL 730 CONTINUE		MAD= 1./57.2957795 MP=(360./ANG)+1.001	NTINE-11 FSI(1) II D.	. 6

Figure 34. Program Listing - AVQUAD, E386RN.

PSI(I)= PSI(I-1)+ ANG PRAD(I)= PSI(I)*RAD 07 77 1=1,NPA 9(J,I)=XLO(I)	622 623 624 625 625
DO 17 K=1.NEM X=K W(J,1)=G(J,1)+XLM(I,K)+COS(X*PRAD(J))+XMM(I,K)*SIN(X*PRAD(J)) 1F(KEY1,NE,99) GO TO 88 UO 86 I=1.NRAD WRITE (6.87) XLO(I),((XLM(I,J),XMM(I,J)),J=1.NHAR)	629 630 631 631
FORMAT (E25.8), (2E25.8)) WRITE (6.8) BOI-81-6H-0M6-RBN-RO,(R(I):1=1,NRAD) FORMAT (4H0B01-E15.6,4H B1-E15.6,5H B11,E15.6,7H CHORD.E15.6,7H 7H OMEGA.E15.6,8H BLADES.F7.0,//25H RADIUS AT START OF TWIST. E15.6,///30x,21HBLADE SECTION LOADING,///7H RADIUS,10x,1H1,14x, 1H2:14x,1H3:14x,1H4:14x,1H5:14x,1H6:14x,1H7:14x;1H8:/8H AZIMUTH,	634 634 635 635 637
DO 9 1=1.NP WRITE (6:10) I.PSI(I),(G(I,K),K=1,NRAD) FORMAT (14,F7.1.8E15.6) ONG=3.14159265*OMG/30, SOS=12.*50S BO1=B01=RAD B11=B11=RAD B11=B11=RAD G=G=RAD	0 1 2 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2
BEGIN MAJOR LOOP ON FIELD POINTS UD 999 II=1.NFP CAPR=CAPRF(II) THETA=THETAF(II) ALFA=ALFAF(II) FORMAT (SFL2.4)	655 655 655 655 655 655 655
WRITE (0122 CAPY) HE AVALTA. FORMAT (1240FIELD POINT,10X,6HRADIUS,EIS.6,5X,7HAZIMUTH,EIS.6,5X, 9HELEVATION,EIS.6,/20X,8HHARMONIC,10X,14HSOUND PRESSURE,ISX, CAPR=12,*CAPR ALFA= RAD&ALFA	658 658 660 661 662
JUNE 18— KANETIELIA JOS 990 KKELIANHAR DO 990 KKELIANHAR DO 990 LJ-1ANT CAPS= SGRT(CAPR*CAPR*R(KK)*COS(ALFA)* COS(PRAD(JJ)-THETA) COS(PRAD(JJ)-THETA) COS(BETA) CBTA=COS(BETA) CBTA=COS(BETA) CBTA=COS(BETA)	666 666 666 667 668 669 670 671

Figure 35. Program Listing - E386RN.

9979 EGRAL (TAREALO) 1 9000-5050-9014 (NY) = (STREMPERBNECH/RIKKI) = (COS(V)/CAPS+TTEMPERBN 1 9000-5050-9014 (NY) = (STREMPECAPS-COS(ALEA/ASTRINGARD(AJ) - THETA + STRIALEA) = 677 1 20017 ANT (NY) (STREMPECAPS-COS(ALEA/ASTRINGARD(AJ) - THETA + STRIALEA) = 679 20017 ANT (NY) (STREMPECAPS-CAPS) (STREMPERBNECH/RIKKI) (COS(V) * TEMPERBNOWG 1 20017 ANT (NY) (STREMPECAPS-CAPS) (STREMPERBNECH/RIKKI) (STREMPERBNOWG 20017 ANT (NY) (STREMPERBNECH/RIKKI) (STREMPERBNE	······································	8 CD COUNT
**************************************	FORMAT TEMP=	675
VESTIONAL SIGNAL STREETH PROBLEM STREETH PROBLEM STREETH PROBLEM STREETH PROBLEM STREETH PROBLEM STREETH STREETH PROBLEM STREETH STREE	V25(JJ)=(@(JJ-KK)#SIN(.5#TEMP#RBN#CH/R(KK))#(COS(V)/CAPS+(TEMP#RBN 1 #OMG/SOS)#SIN(V))#(SBTA#COS(ALFA)#SIN(PRAD(JJ)-THETA)#SIN(ALFA) #	677 678
CALL SHORM WERN AND CHARACOS (ALEADS SHIPPRADILAU)—THETA + SIN (ALEAD + SCHETA + SCHET	2CBTA)+R(KK))/(TEMP+CAPS) V2BI(CL)H(G(LC*K)+SIN(*S+TEMP+RBN+CH/R(KK))+(COS(V)+TEMP+RBN+ONG	679
CONTRINGE (**AL. SINCOR(**P**PAD(2)**V25 ,AR*IERR) **ELIERR.**(**AL. SINCOR(**AL. SINCOR(*	1. /SOS-SIN(Y)./CAPS) # (SBTA*COS(ALFA) #SIN(PRAD(JJ) -THETA) +SIN(ALFA) #	681
VASI (1971-19211) (ALL SINCOR (NP-PRAD(2), V25, AR, IERR) (ALL AND (MACAD (MACAD R) (MACAD R) (ALL AND (MACAD R) (ALL AND (MACAD R) (ALL AND (MACAD R) (ALL AND (MACAD R) (ALL AND (MACAD R) (ALL AND (MACAD R) (ALL AND (MACAD R) (ALL AND (MACAD R) (ALL COMMITTEE (MACAD R) (ALL AND (MACAD R) (MACAD R)	99 CONTINUE	683
ELEERR .E. O. WRITE(6.09418) FORMAT(.//25x.23HERROR IN SINCOR, IERR=0 ///) VORTHERR .E. O. WRITE(6.09418) IF(IERR .E. O. WRITE(6.09418) IF(IERR .E. O. O. WRITE(6.09418) IF(IER .E. O. O. WRITE(6.095) IF(IER .E. O. O. O. O. WRITE(6.095) IF(IER .E. O. O. WRITE(6.095) IF(IER .E. O.	V25(WP) = V25(1)	684 486 584
FORMATI///25.23.HERROR IN SIMOR, IERR=0 /// VOURKIE LAR (ALL SIMCOR(MP, PRADIZ), V251, RR. IERR) IFIGETER, EG. 0) WRITE (6.9976) V81KK1, (V25(1), I=1,NP) CONTINUE (6.997) WRITE (6.9975) PRTAI (1.05(1), 1, KK=1, NRAD) IFIGETER, EG. 99) WRITE (6.9975) PRTAI (1.05(1), 1, KK=1, NRAD) IFIGETER, EG. 99) WRITE (6.9975) PRTAI (1.05(1), 1, KK=1, NRAD) FORMATI (25.6, 12.5, 1	RAD(2), V25	989
CALL ANGURE (18. 19. MRITE (6. 9976) VBIKKI. (VZSIII. III.NP) IF (IERR .EG. 9) MRITE (6. 9976) VBIKKI. (VZSIII. III.NP) IF (IERR .EG. 99) MRITE (6. 9976) VBIKKI. (VZSIII. III.NP) FORMAT (7/E25. 8/7 (5E2.8) (5E2.8) CALL ANGUAD (18. A. 19. PRITA) IF (KRYI.EG. 99) WRITE (6. 9975) PRITA! (VBIKK). KK=1. NRAD) IF (KRYI.EG. 99) WRITE (6. 9975) PRITA! (VBIKK). KK=1. NRAD) IF (KRYI.EG. 99) WRITE (6. 9975) PRITA! (VBIKK). KK=1. NRAD) IF (KRYI.EG. 99) WRITE (6. 9975) PRITA! (VBIKK). KK=1. NRAD) IF (KRYI.EG. 99) WRITE (6. 9975) PRITA! (VBIKK). KK=1. NRAD) IF (KRYI.EG. 99) WRITE (6. 9975) PRITA! (VBIKK). KK=1. NRAD) IF (KRYI.EG. 99) WRITE (6. 9975) PRITA! (VBIKK). KK=1. NRAD) IF (KRYI.EG. 997) WRITE (6. 9975) PRITA! (VBIKK). KK=1. NRAD) WRITE (6. 997) WRITE (6. 997) WRITE (6. 997) WRITE (6. 997) WRITE (6. 997) WRITE (6. 997) WRITE (6. 997) WRITE (6. 997) WRITE (6. 997) WRITE (6. 997) WRITE (6. 997) WRITE (6. 997) WRITE (6. 997) WRITE (6. 997) WRITE (6. 997) IN THE EQUATION F (X) OVER A RANGE (A.B) WRITE (6. 997) WRITE (6. 997) WRITE (6. 997) SIMPSONS RULE WITH A CORRECTION FACTOR INCORPORATED IN THE EQUATION F (X) OVER A RANGE (7. NP A RA	FORMATI(//25x,23HERROR IN SIMCOR, IERR=0	687 688
	VO(KK)=AR	689
	CALL SIMCOR(NP)PRAD(2)+V251,AR,IERR) IF(IERR .EG. 0) WRITE(6,8418)	690
FIGET E 69 99 WITE (69876) VBICK() (V251(1) IIINP) COLL AVOUND (WADD.R.V8.PRTAR) FORMAT (7.625.8) WRITE (6.9975) RTAR.(V81(KK).KK=1.NRAD) FORMAT (7.625.8) WRITE (6.9975) RTAR.(V81(KK).KK=1.NRAD) FORMAT (2.62.8) WRITE (6.9975) RTAR.(V81(KK).KK=1.NRAD) FORMAT (2.62.8) WRITE (6.9975) RTAR.(V81(KK).KK=1.NRAD) FORMAT (2.62.12.5x.2620.8) FORMAT (2.62.12.5x.2620.8) FORMAT (2.64.12.8) FO	VBI (KK)=AR	695
CONTINUE CALL AVONDO (NRAD.R.VB.PRTAR) CALL AVONDO (NRAD.R.VB.PRTAR) CALL AVONDO (NRAD.R.VB.PRTAR) IF (KETI.E9.99) WRITE (6.9875)PRTAR; (VB(KK),KK=1,NRAD) INTECCONTINUE BUGGGGATC SURCOR,SIMCOR SUCCONTINUE FOR SIMCOR (N.H.Y.XINI')IERR) PURPOSE SIMPSONS RULE WITH A CORRECTION FACTOR INCORPORATED SIMPSONS RULE WITH A CORRECTION FACTOR INCORPORATED SIMPSONS RULE WITH A CORRECTION FACTOR INCORPORATED IN THE EQUALION IS USED WITHOUT THE CORRECTION FACTOR IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IN THE EXPRESSION FACTOR INCORPORATED IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IN THE CORRECTION FACTOR INCORPORATED IN THE LOWER BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY IF (N-1) IS ONLY DIVISIBLE BY	WRITE (6,9876)	469
CALL AVOIDD (MRAD-R.VB.PRTAR) CALL AVOIDD (MRAD-R.VB.PRTAR) IF (KEYI.EB.99) WRITE (6.985) PRIAR.(VB(KK).KK=I.NRAD) IF (KEYI.EB.99) WRITE (6.985) PRIAR.(VB(KK).KK=I.NRAD) IF (KEYI.EB.99) WRITE (6.985) PRIAR.(VB(KK).KK=I.NRAD) FORMAT (258228-540-64) FORMAT (258-18-55-64-18-59) FORMAT (258-18-55-18-18-18-18-18-18-18-18-18-18-18-18-18-	FORMAT (//E25.8/.(5E25.8/))	695
LE (KEYLEG.99) WRITE (6.9873) PRIAR; (VB(KK), KK=1.NRAD) 1F (KEYLEG.99) WRITE (6.9873) PRIAR; (VB(KK), KK=1.NRAD) 1F (KEYLEG.99) WRITE (6.9873) PRIAL; (VBI(KK), KK=1.NRAD) 1F (KEYLEG.99) WRITE (6.9873) WRITE (6.9873) WRITE (6.997) WRITE (6.997) 1F (KEYLEG.997) WRITE (1.997) WRI	CALL AVOIDED	969
IF (KEYILEG-99) WRITE (6:9975) PRIAM; (VB(KK) KK=L,NRAD) F (KEYILEG-99) WRITE (6:9975) PRIAM; (VBI(KK) KK=L,NRAD) F (KEZ5-8, /4E25-8, /4E25-8) F (KEZ5-8-74E25-8, /4E25-8) F (KEZ5-8-74E25-8, /4E25-8) F (KEZ5-8-74E25-8) F (KEZ5-8-74E2-8) F (KEZ5-8-	CALL AVOUAD (NRAD,R, VBI, PRTAI)	869
PRIATION FORMAT (//EES.8/7EES.	KEYL E9.99) WRITE	669
PRIATE SOURCE STANDARD SOURTINE SOURTINE SOURTINE SOURTINE SOURT (25X-12-5X-220-0) WHITE (6.997) W.PRIA-SPL FORMAI (25X-12-5X-2E20-0) FORMAI (25X-12-5X-2E20-0) FORMAI (25X-12-5X-2E20-0) FORMAI (25X-12-5X-2E20-0) FORMAI (25X-12-5X-2E20-0) FORMAI (25X-12-5X-2E20-0) BUG-6ATC	FORMAT (//E25.8,/4525.	701
FORMAT (25X,12,5X,2E20,8) CONTINUE B0=6ATC1 B1C=6ATC2 B1S=6ATC3 6AMA=6ATC4 OMEG=5ATC5 FOR SIMCOR, SIMCOR FOR SIMCOR, SIMCOR FOR SIMCOR, SIMCOR FOR SIMCOR, SIMCOR FOR SIMCOR, SIMCOR FOR SIMCOR FOR SIMCOR, SIMCOR FOR SIMCOR, SIMCOR FOR SIMPSONS RULE WITH A CORRECTION FACTOR INCORPORATED IN THE EQUATION IS USED WITHOUT THE CORRECTION FACTOR SIMPSONS RULE IS USED WITHOUT THE CORRECTION FACTOR IF (N-1) IS ONLY DIVISIBLE BY 2	PRTA=(.03582245+C4PR/CH) + SQRT(PRTAR++2+PRTA1++2)	702
FORMAT (25%, 12,5%, 2620,8) CONTINUE BUG=GATC1 BIC=GATC2 BIS=GATC3 GAMA=GATC4 OMEG=GATC5 GAMCGA-SIMCOR SIMCOR-SIMCOR FOR SIMCOR FOR	WRITE (6,997) M.PRTA.SPL	703
B0=6ATC1 B1C=6ATC2 6AMA=6ATC4 OMEG=6ATC5 NETURN LND LND ENCOR, SIMCOR SUBROUTINE SIMCOR SUBROUTINE SIMCOR TO INTEGRATE A FUNCTION F(X) OVER A RANGE (A,B) TO INTEGRATE A FUNCTION F(X) OVER A RANGE (A,B) METHOD SIMPSONS RULE WITH A CORRECTION FACTOR INCORPORATED IN THE EQUATION IS USED IF (N-1) IS DIVISIBLE BY BOTH 2 AND 4 SIMPSONS RULE IS USED WITHOUT THE CORRECTION FACTOR IF (N-1) IS ONLY DIVISIBLE BY 2	FORMAT	705
BIC=6ATC2 BIS=6ATC3 GAM=6ATC4 OMEG=6ATC5 NETURN LND LND SIMCOR, SIMCOR SIMCOR, SIMCOR SIMCOR, SIMCOR		706
BISSONS RULE WITH A CORRECTION FACTOR SIMPSONS RULE WITH A CORRECTION FACTOR INCORPORATED IN THE EQUATION IS USED IF (N-1) IS DIVISIBLE BY BOTH 2 AND 4 SIMPSONS RULE IS USED WITHOUT THE CORRECTION FACTOR IN THE SOURT SONLY DIVISIBLE BY BOTH 2 AND 4 SIMPSONS RULE IS USED WITHOUT THE CORRECTION FACTOR IF (N-1) IS ONLY DIVISIBLE BY 2	BIC=6ATC2	708
OMEG=6AICS NETURN LND FOR SIMCOR, SIMCOR SUBROUTINE SIMCOR (N.H.Y.XINT, IERR) PURPOSE TO INTEGRATE A FUNCTION F(X) OVER A RANGE (A.B) METHOD SIMPSONS RULE WITH A CORRECTION FACTOR INCORPORATED IN THE EQUATION IS USED IF (N-1) IS DIVISIBLE BY BOTH 2 AND 4 SIMPSONS RULE IS USED WITHOUT THE CORRECTION FACTOR IF (N-1) IS ONLY DIVISIBLE BY 2	B12=6A1C3 GAMA=GATC4	709
END FOR SIMCOR.SIMCOR SUBGOUTINE SIMCOR (N.H.Y.XINT.IERR) PURPOSE TO INTEGRATE A FUNCTION F(X) OVER A RANGE (A.B) METHOD SIMPSONS RULE WITH A CORRECTION FACTOR INCORPORATED IN THE EQUATION IS USED IF (N-1) IS DIVISIBLE BY BOTH 2 AND 4 SIMPSONS RULE IS USED WITHOUT THE CORRECTION FACTOR IF (N-1) IS ONLY DIVISIBLE BY 2	OMEG-6AICS	711
SUBCORSINCOR SUBCOR (N.H.Y.XINT.IERR) PURPOSE TO INTEGRATE A FUNCTION F(X) OVER A RANGE (A.B) METHOD SIMPSONS RULE WITH A CORRECTION FACTOR INCORPORATED IN THE EQUATION IS USED IF (N-1) IS DIVISIBLE BY BOTH 2 AND 4 SIMPSONS RULE IS USED WITHOUT THE CORRECTION FACTOR IF (N-1) IS ONLY DIVISIBLE BY 2	E NO	713
PURPOSE TO INTEGRATE A FUNCTION F(X) OVER A RANGE (A,B) METHOD SIMPSONS RULE WITH A CORRECTION FACTOR INCORPORATED IN THE EQUATION IS USED IF (N-1) IS DIVISIBLE BY BOTH 2 AND 4 SIMPSONS RULE IS USED WITHOUT THE CORRECTION FACTOR IF (N-1) IS ONLY DIVISIBLE BY 2	SUBROUTINE SIMCOR	714
TO INTEGRATE A FUNCTION F(X) OVER A RANGE (A,B) METHOD SIMPSONS RULE WITH A CORRECTION FACTOR INCORPORATED IN THE EQUATION IS USED IF (N-1) IS DIVISIBLE BY BOTH 2 AND 4 SIMPSONS RULE IS USED WITHOUT THE CORRECTION FACTOR IF (N-1) IS ONLY DIVISIBLE BY 2	PURPOSE	716
METHOD SIMPSONS RULE WITH A CORRECTION FACTOR INCORPORATED IN THE EGUATION IS USED IF (N-1) IS DIVISIBLE BY BOTH 2 AND 4 SIMPSONS RULE IS USED WITHOUT THE CORRECTION FACTOR IF (N-1) IS ONLY DIVISIBLE BY 2	TO INTEGRATE A FUNCTION F(X) OVER A	717
SIMPSONS RULE WITH A CORRECTION FACTOR INCORPORATED IN THE EQUATION IS USED IF (N-1) IS DIVISIBLE BY BOTH 2 AND 4 SIMPSONS RULE IS USED WITHOUT THE CORRECTION FACTOR IF (N-1) IS ONLY DIVISIBLE BY 2		719
IN THE EQUATION IS USED IF (N-1) IS DIVISIBLE BY BOTH 2 AND 4 SIMPSONS RULE IS USED WITHOUT THE CORRECTION FACTOR IF (N-1) IS ONLY DIVISIBLE BY 2	SIMPSONS RULE WITH A CORRECTION	721
SIMPSONS RULE IS USED WITHOUT THE CORRECTION FACTOR IF (N-1) IS ONLY DIVISIBLE BY 2	IN THE EQUATION IS USED IF (N-1	723
SIMPSONS RULE, IS USED WITHOUT THE CORRECTION FACTOR If (N-1) IS ONLY DIVISIBLE BY 2		725
	SIMPSONS RULE IS USED WITHOUT THE IF (N-1) IS ONLY DIVISIBLE BY 2	726
		728

Figure 36. Program Listing - E386RN, SIMCOR.

.	2 3 4 5	CD COUNT	
o o o	IF (N-1) IS NOT DIVISIBLE BY 2 THIS IMPLIES THAT N IS EVEN AND THIS SUBROUTINE CAN NOT BE USED.	730	
ט ט ט	CALLING SEQUENCE	732	
o c	CALL SIMCOR (N'H'Y'XINT, IERR)	734	
ט ט נ	DESCRIPTION OF PARAMETERS	736	
יטנ	NNUMBER OF POINTS THAT ARE TAKEN OVER THE CURVE	738	
יטנ	H -CONSTANT INTERVAL BETWEEN THE POINTS	740	
י ט נ	Y -SUPPLIED FUNCTION	742	
ט ט נ	XINT-TOTAL AREA UNDER THE CURVE BETWEEN A AND B	140	
	CODE = 0 : (N-1) N	745	
) U U :	IS DIVISIBLE	750	
ی	DIMENSION Y(1)	752	
	ALMN 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	754	
	T Y(1) + 4.4 Y(N-1) + Y	756	
10	NO 10 I = 2.N3.2	758	+
	O * XINT	760 761 762	
	L= Y(1) + 4.* Y(N-2) N-6	763	
20	D. 2D I = 3.N6.4 XINITE XINITE 4.* Y(I) + 2.* Y(I+2) XINITE 0.* L/4 - YEAT	765	
	XINT + (XIN	768	
	3	077	· dayer day management of the first of the f
DIXE	FOR START, START SUBROUTINE START COMMON /TEMPUS/ TIME, COUNT	772 773 777	
	INTEGER COUNT UATA COUNT /0/ CALL RIMINS (TIME)	775	
	COUNT = COUNT + 1 CALL CLOCK RETURN	778 779 780	
9110	FOR CLOCK, CLOCK	782	

Figure 37. Program Listing - SIMCOR, START, CLOCK.

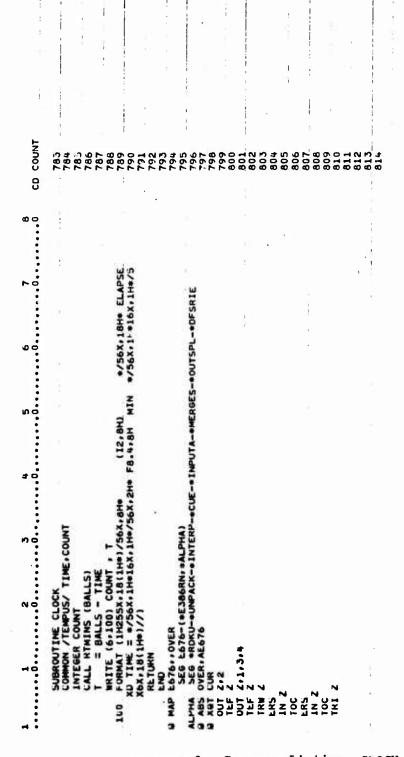


Figure 38. Program Listing -CLOCK, End.

Unclassified								
Security Classification								
DOCUMENT CONTROL DATA - R & D								
(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)								
ORIGINATING ACTIVITY (Corporate author)								
Sikorsky Aircraft								
Division of United Aircraft Corporation		28. 44007						
Stratford Connecticut								
HELICOPTER ROTOR ROTATIONAL NOISE PREDICTION AND CORRELATION VOLUME II - DOCUMENTATION OF NOISE PREDICTION COMPUTER PROGRAM								
4. DESCRIPTIVE NOTES (Type of report and inclusive dates)								
Final								
S. AUTHOR(S) (First name, middle initial, last name)								
Ronald G. Schlegel								
William E. Bausch								
S REPORT DATE	Tre. TOTAL NO. OF	PAGES	7b. NO. OF REFS					
November 1970	1							
M. CONTRACT OF GRANT NO.		DE ENTERON SECURITY CLASSIFICATION Unclassified 2b. GROUP RELATION VOLUME II - CONTREPORT NUMBERIS) SE Technical Report 70-1B EPORT NO(5) (Any other numbers that may be assigned) th prior approval of U.S. Arr a 23604. NO MILITARY ACTIVITY Aviation Materiel Laboratories is, Virginia 23604 Se documented. The program was rate methods for predicting orm inflow over the rotor disc. Juare sound pressure level for point in the near or far field culated either from a rectangular red chordwise distribution. The measured) chordwise distribution is report concentrated on a						
DA 44-177-AMC-448(T)								
A. PROJECT NO.	USAAVLABS TO	echnical R	leport 70-1B					
Task 1F162203A14801			•					
c.	USAAVLABS Technical Report 70-1B **D. OTHER REPORT NO(5) (Any other numbers that may be assigned this report) controls, and each transmittal to foreign the only with prior approval of U.S. Art							
	15000 31600							
d.	<u> </u>							
This document is subject to special export governments or foreign nationals may be mad Aviation Materiel Laboratories, Fort Eustis	de only with p s, Virginia	prior appr 23604.	coval of U.S. Arr					
11. SUPPLEMENTARY NOTES	12. SPONSORING MI	LITARY ACTIV	ITY					
Volume II of 2 volumes	U.S. Army Aviation Materiel Laboratories Fort Eustis, Virginia 23604							
13. ABBTRACT								
A computer program for rotational noise prodeveloped as a part of a study to develop me rotational noise levels under conditions of	nore accurate	methods f	for predicting					
The computer program will calculate the room up to the 10th harmonic of rotor noise at a outside of the rotor disc. Noise levels calchordwise distribution of pressure or from equations for noise prediction using the arrange derived in Volume I of this report. All helicopter rotor, the analytical results and	any field poin an be calcular the measured rbitrary (meas Lihough this	nt in the ted either chordwise sured) cho report con	near or far field r from a rectangular e distribution. The ordwise distribution accentrated on a					

Unclassified

Security Classification						
14.	LINK A		LINK B		LINKC	
KEY WORDS	ROLE	WT	ROLE	WT	ROLE	WT
	1		1			
		}	ł	1		
Chordwise Distribution	j		i		l	!
Computer Program Helicopter Rotor Noise Noise Prediction	}		[1	ì
Helicenter Poter Noise	1	ł	İ	i		i
nelicopter kotor noise			1	1	ł	l
Noise Prediction	1	ĺ	i			l
Rotational Noise Levels	1 .	l	1			ĺ
Rotor noise	1	1	1		l	l
		[f	1	1	i
		i			1	i
			İ	l	I	l
	1 .			ŀ		
•	1				ì	l
	1				1	
					1	
	1					
	1		j			
	1 1]		J I	
	!!					
	1]	
	! I		! !		i i	
	1 1		, ,		i 1	
	!		1 1			
	į į		ĺĺ		l 1	
	[]	,	1		i i	
• •	1		1)	
,	1 1		i i		1 1	
]		1 1	
			1 1		1	
•						
			ĺ			
					1	
			ŀ			
	1				,	
					ĺ	
	1					
		- 1				
		l			ł	
3					l	
	1					
	i					
				1		
	İ		ł			
	ŀ			1		
		1				
					}	
į daras ir d	i	I			1	

Unclassified
Security Classification